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A NEW FALLOUT TRANSPORT CODE FOR THE
Delfic System: The Diffusive Transport
Module. Supplement

Hillyer G. Norment

Mount Auburn Research Associates, Incorporated

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THE DIFFUSIVE TRANSPORT MODULE - SUPPLEMENT

Prepared by

H. G. Norment

MT. AUBURN RESEARCH ASSOCIATES, INC.
385 Elliot Street
Newton, Massachusetts 02164

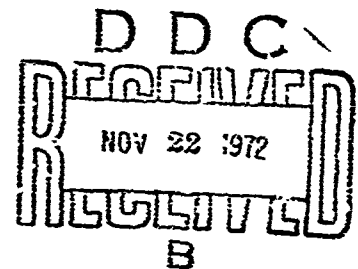
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ABSTRACT

The Diffusive Transport Module of the new DELFIC fall-out prediction system has undergone additional development since publication of its description in DASA 2669. This supplement to DASA 2669 describes these developments and presents amendments and corrections to the code and its documentation. Complete FORTRAN statement listings of sub-routines that have been substantially changed are included.

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1. INTRODUCTION

Since publication of DASA 2669*, development and application of the DELFIC Diffusive Transport Module (DTM) has continued. A few revisions to the model have been made, several of them of major importance. In addition, some hidden "bugs" have been uncovered and corrected. In this supplement to DASA 2669 we describe the important model revisions, and amend the documentation. We also correct errors in the documentation, and provide FORTRAN statement listings of subroutines that have been changed substantially.

* H. G. Norment and E. J. Tichovolsky, "A New Fallout Transport Code for the DELFIC System: The Diffusive Transport Module," ARCON Corporation Report R71-1W, DASA 2669 (1 March 1971), AD 727 613.

2. MODEL REVISIONS

2.1 Initial Parcel Description

Fallout parcels are taken to be distributed in the horizontal about their centers of mass by a Gaussian density function. The initial Gaussian standard deviation was set equal to the parcel radius that was received via tape IPARIN from the Cloud Rise-Transport Interface Module. This has been changed so that the initial standard deviation is one-half the input parcel radius. (Compare subroutine SPRVS card 81 of DASA 2669 with SPRVS card 94 of this supplement.)

2.2 Simple Advection-Plus-Settling

In some cases, it is desirable to transport fallout in a simple advection-plus-settling mode; that is, without accounting for diffusion in the vertical. In this mode, integration of Eq. (16) is bypassed, and the parcel trajectory is computed via Eq. (32). As actually employed in the original DTM, Eq. (32) was modified to the form

$$\vec{r}_c = \vec{r}_i + \frac{1}{\langle \vec{f} \rangle - \langle w \rangle} \sum_{z_i}^{z_g} \vec{U}(x, y, z, t) \Delta z ,$$

where the average settling speed, $\langle f \rangle$, was taken to be

$$\langle f \rangle = \frac{f(z_i) + f(z_g)}{2} .$$

and $\langle w \rangle$ was an average vertical air velocity. For cases where $z_i - z_g$ is large, there can be significant differences in the particle settling speeds in the upper layers compared with those in the lower layers. When, in addition, there is large wind shear in the vertical,

Preceding page blank

it becomes necessary to use settling speeds that are computed individually for each wind layer instead of an average settling speed. The code has been changed so that this is done.

Major changes have been required in several programs. The most extensive changes are in subroutines SPRVS and TRANP. A new array, CAVS(KBHF), is created to store a table of particle settling speeds; it contains an entry for each wind layer.

Before a parcel is transported via this mode, a test is made to determine if the parcel can impact in the time allowed for transport. This test is simplified by using the knowledge that all parcels comprised of particles of a particular size class are processed sequentially in one group. Thus, as each new particle size class is encountered, the altitude above which these particles cannot impact is computed. Then, any parcel in the group whose base is above this altitude is bypassed. To perform the altitude limit calculation, an average vertical wind velocity is needed for each wind layer. To accommodate this, the array WAVG(LTIME) was changed to the array WAVG(KBHF,LTIME).

3. DOCUMENTATION REVISIONS

Revisions and corrections are intermixed and listed in order of their encounter in DASA 2669.

Page 27, Eq. (23):

$$t_1 = 4c_3 \left(\frac{\sigma_{t_i}^2}{\varepsilon} \right)^{1/3} \quad (23)$$

Page 27, line 16:

In our application, σ_{t_i} is taken to be one-half of the radius of a cloud wafer as recorded

Page 44, line 3:

where the summation is over the N data with the largest f_i , and the weighting factors,

Page 44, lines 6 and 7:

The parameters α , β , and N are specified by the user and the x_i and y_i are relative to the n-th lattice cell center. The calculations of the f_i are performed so that whenever a factor in Eq. (39) is found to

Page 44, lines 9 and 10:

than the total number of observations, M, only the N observations with the largest f_i relative to the n-th lattice cell center are considered in the calculations.

Page 45, lines 8-12:

list, two tables of settling rates for this particle are computed. One table contains an entry for each altitude increment used in the numerical integration of Eq. (16).

The other table contains an entry for each of the larger altitude increments that are used to resolve the wind and turbulence fields. These same tables are used through transport for this parcel and the remainder of the parcels in the first group. When the first parcel of the second group is selected, new tables are computed, and so on.

Page 49, Eq. (45):

$$\frac{G_j^{n+1} - G_j^n}{\Delta t} = \frac{1}{2(\Delta z)^2} \left[(K_{j+1} + K_j)G_{j+1}^n - (K_{j+1} + 2K_j + K_{j-1})G_j^n + (K_j + K_{j-1})G_{j-1}^n \right] + \frac{1}{\Delta z} \left[(f_{j+1} - w_{j+1})G_{j+1}^n - (f_j - w_j)G_j^n \right] \quad (45)$$

Page 53, following Eq. (65):

where in the code K_{J+1} is taken to be equal to K_J .

Page 66, paragraphs 1 and 2:

Beginning at its input location and time, the parcel base or top is transported via local winds in the cell of its residence. At the same time it settles at a speed that is computed for the altitude at the center of the wind cell of its residence. When it passes through a wind cell boundary or a time boundary, the wind and settling speed are changed to those of the new cell or update. This continues until ground impaction occurs or until an extreme wind field or time boundary is encountered. The calculation requires one step for each cell through which the base or top passes.

When an extreme boundary is encountered by a top or base, the location and time of the encounter is recorded. These values are used in the definition of the deposit increment as described on page 70. The altitude of a deposit increment is always recorded as the arithmetic average of the impact

altitudes of its top and base. Thus, the recorded altitude of a deposit increment that has reached an extreme boundary can be well above the deposition plane.

Page 71, Figure 9:

The quantity labeled $\sigma(\perp)$ that lies to the left of the deposit increment ellipse should be replaced by $\sigma(\perp)_d$.

Page 88, lines 10 and 11:

DFZ. An area-weighted average vertical wind, $WAVG(KBH, LTIM)$, is derived from array WFZ for each altitude layer and update. Likewise, a volume-weighted

Page 88, equation for DKAV:

$$DKAV = \sum_{KBH=1}^{KBHX-1} \frac{DFZ(KBH, NDATA, LTIM) * (ZBH(KBH+1) - ZBH(KBH))}{ZBH(KBHX) - ZBH(1)}$$

Page 88, lines 27 and 28:

out on ISOUT. In a parallel operation the quantities $WAVG(KBH, LTIM)$, which are area-weighted vertical wind velocities for each wind layer and update, are computed and printed out on

Page 96, line 25:

in the horizontal $RWFR(J)/2.0$;

page 97, line 12:

$ZPAR(J)$, $PSAM(J)$, $RWFR(J)/2.0$, $DWFR(J)$, $ZLWF(J)$, and $VWFR(J)$ are

Page 98, line 2:

for further details.) Also computed are the settling speeds,

CAVS(KBH), for each altitude, and the altitude, ZLIM, above which deposition is impossible, via gravity settling in the specified wind field, for particles in the particular size class being considered.

Page 100, last line:

CAV = CAV - WAVGK

Page 101, first line:

WAVGK and DAVG(1) are the average vertical components of wind

Page 101, line 15:

ground by advection at fall rates CAVS(KBHF) via a call to subroutine ADVEC.

Page 101, line 23:

limit: i.e., whenever $ZLOW \geq ZLIM$. The comment

Page 110, lines 16-19:

also obtained via the COMMON area QPARM. The particle settling speeds, CAVS(KBHF), and area-weighted vertical air velocities, WAVG(KBHF,LTIMF), for each wind layer, are obtained

Page 110, line 27:

parcel base is advected, while settling at speeds CAVS(KBH) - WAVG(KBH,LTIM), from position (XP,YP,ZP =

Page 110, line 29:

TOL. The standard deviations of the

Page 110, line 33:

parcel top is advected, while settling at speeds $CAVS(KBH) -$
 $WAVG(KBH,LTIM)$, from position $(XP,YT,$

Page 111, line 2:

at time TOU . The standard

Page 111, second paragraph:

After both base and top of a parcel have been transported, the arithmetic average of the two impact times and impact altitudes are recorded for the deposit increment (as shown on the next page). In the event that the base or top encounters an extreme wind field or time boundary during transport, subroutine $TRANP$ returns the coordinates of the encounter point. Therefore, the altitude recorded for a deposit increment can be well above the deposition plane.

Page 111, third paragraph, lines 4 and 5:

Is considered superfluous whenever ZP differs from $ZDEP$ by less than 0.1. Instead, XOL , YOL , ZOL , TGL , $SIGXI$, $SIGYL$,

Page 122, line 28:

When vertical diffusive transport is employed, the computation of horizontal parcel advection is based on the

Page 123, insert between the second and third paragraphs:

For transport via simple advection plus settling, $TRANP$ is called by subroutine $ADVEC$ with $KRIP=0$ (otherwise $KRIP=1$). The parcel top or bottom is transported stepwise through the vertical layers between ZP and $ZDEP$ via the layerwise mode (see below). In each layer, with index KBH , the vertical velocity is

$WBAR = WFZ(KBH, NDATA, JTIM) - CAVS(KBH)$

and $KAY = -.1$. TSEG is computed as shown by the equation in the preceding paragraph.

Page 123, third paragraph, line 3:

is traversed at a time. This mode is mandatory for transport via simple advection plus settling, or when a parcel trajectory

Page 125, line 6:

The rapid computation mode is employed for vertical diffusive transport when

Page 145, insert at the end of the Input Data Card 4 discussion:

To preempt vertical diffusive transport, set $KX=1$ and set ZMAX arbitrarily large. This causes all parcels to be transported via the simple-advection-plus-settling mode (Eq. (32)). Of course, horizontal diffusive growth of parcels is accounted for in any case.

Page 146, line 14:

CSKIP - 0.1

Page 152, line 8:

HITIME. If the vertical diffusive mode of transport is used, the KBHX'th base should be above or at the top of the transport space as this top is specified by ZMAX.

Page 156, Table 4, Record Number 12, line 6 under Content:

size class central diameter (μm), mass of fallout (kg)

Page 154, to the end of paragraph 1 add:

However, the turbulent energy dissipation rates can be input only for the horizontal directions; for the vertical direction Fickian diffusivities always are input, regardless of which type of data are input for the horizontal.

4. CODE REVISIONS

4.1 Single Card Changes

Addition of the arrays CAVS(KSHF) and WAVG(KSHF,LTIME) requires revisions in DIMENSION statements and subroutine argument lists. However, complete FORTRAN statement listings are given in this supplement for all subroutines that require these revisions.

Subroutine EDUN, card 27:

```
CALL NEST (NET, NETSU, XO, YO, NDATO, XL, XR, YL, YU, ICF,  
JCF, NCF)
```

Subroutine DUMPER:

Place card 33 in its proper position.

Subroutine NEST, insert between cards 20 and 21:

```
DIMENSION NET(ICF, JCF), NETSU(NCF)
```

4.2 FORTRAN Statement Listings

Complete FORTRAN statement listings are given for the following subroutines. These subroutines are operational on the UNIVAC 1108.

<u>Subroutine</u>	<u>Page</u>
C31M	13
ADMIN	18
ADVEC	21
AMBNT	23
SPRVS	26
TRANP	32

The machine used to prepare these listings prints a # symbol to represent a 4-8 punch; this symbol should be an apostrophe ('). In FORMAT and DATA statements, the apostrophe is used to define Hollerith character fields.

C	SEPTEMBER 1971	C31M	1
C	C31M IS THE MAIN PROGRAM WHICH DIRECTS THE DIFFUSIVE TRANSPORT	C31M	2
C	MODULE OPERATIONS. THE OBJECT-TIME DIMENSIONS ARE SET IN C31M.	C31M	3
C	THESE DIMENSIONS AND THEIR RESPECTIVE ARRAYS ARE	C31M	4
C	KKF - AA, BB, CC, DENOM, E, F, Q, R, DIFF, ZHT	C31M	5
C	LTIME - TIMUP, DAVG, WAVG	C31M	6
C	KBHF - ZBH, ZCH	C31M	7
C	NDATF - KTOFO	C31M	8
C	KBHF, NDATF, LTIME - DFZ, DXSUM, DYSUM, USUM, VSUM, WFZ, RSUM	C31M	9
C	ICF, JCF - NET	C31M	10
C	NCF - NETSU	C31M	11
C	MARF - MARY	C31M	12
C	NATF - ALT, ATEMP, RFO	C31M	13
C	DATA LITERALS MUST BE INSERTED IN THE DIMENSION STATEMENTS AND IN	C31M	14
C	THE RIGHT HAND SIDES OF THE ARITHMETIC STATEMENTS IN WHICH THE	C31M	15
C	ABOVE VARIABLE NAMES APPEAR.	C31M	16
C	***** GLOSSARY *****	C31M	17
C	AA(K) - EQUALS $S2*(DIFF(K+1)+DIFF(K))+S1*F(K+1)$	C31M	18
C	ALT - ALTITUDES FOR ATMOS. DENSITY AND VISCOSITY TABLE	C31M	19
C	ATEMP - DYNAMIC VISCOSITY OF AIR DATA VECTOR FOR ATMOS. TABLE	C31M	20
C	BB(K) - EQUALS $S2*(DIFF(K+1)+2.*DIFF(K)+DIFF(K-1))+S1*F(K)$	C31M	21
C	CAV - AVG. FALLRATE USED IN COMPUTING PDEST. IT APPLIES MID WAY	C31M	22
C	FROM PARCEL TOP TO ZMIN.	C31M	23
C	CAVS - PARTICLE FALL RATE FOR EACH ATMOS. STRATUM	C31M	24
C	CC(K) - EQUALS $SI*(DIFF(K)+DIFF(K-1))$	C31M	25
C	CROSS - CROSSWIND CROSSING TRAJECTORIES CORRECTION TO TURB.	C31M	26
C	CSKIP - TOTAL FRACTIONAL PARCEL DEPOSITION THRESHOLD	C31M	27
C	DAVG - AVG. ATMOS. VERT. TURB. PER UPDATE DATA VECTOR	C31M	28
C	DENOM(K) - EQUALS $1. - THETA*(BB(K)-CC(K)*E(K-1))$	C31M	29
C	DEP - DEPOSITED FRACTIONAL MASS INCREMENT	C31M	30
C	DIFF(K) - VERT. DIFFUSIVITY AT K-TH SMALL ALTITUDE INCREMENT	C31M	31
C	DFKXS1 - VERTICAL DIFFUSIVITY AT ALTITUDE INCREMENT KX-1	C31M	32
C	DFZ - TURBULENCE Z COMPONENT 3-DIM. DATA ARRAY	C31M	33
C	DTNCR - RATE OF CHANGE OF FRACTIONAL MASS DEPOS. RATE THRESH.	C31M	34
C	DOPEN - MASS DEPOSITION RATE THRESHOLD	C31M	35
C	DOWN - DOWNWIND CROSSING TRAJECTORIES CORRECTION TO TURB.	C31M	36
C	DT - SMALL ITERATION TIME STEP FOR VERT. DIFF. DIFF. EQ.	C31M	37
C	DNAF - PARCEL VERT. THICKNESS BEFORE ADVECTION	C31M	38
C	DXSUM - TURBULENCE X COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY	C31M	39
C	DYSUM - TURBULENCE Y COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY	C31M	40
C	DZ - SMALL ALTITUDE INCREMENT FOR VERT. DIFF. DIFF. EQ.	C31M	41
C	DZMIN - MINIMUM VALUE OF DZ	C31M	42
C	E(K) - EQUALS $THETA*AA(K)/DENOM(K)$	C31M	43
C	EDDY - RATIO OF LAGRANGIAN TURBULENCE TIME SCALE TO EULERIAN	C31M	44
C	TURBULENCE LENGTH SCALE	C31M	45
C	EFFLUX - UPPER EFFLUX FRACTIONAL MASS	C31M	46
C	F(K) - IN SUB. DIFFE, WORKING SPACE IMPLICIT METHOD DATA VECTOR.	C31M	47
C	IN SUB. AMBNT, WORKING SPACE FOR VERTICAL VELOCITIES	C31M	48
C	FAV - MID-ATMOS. AVG. FALLRATE. USED IN CROSSING TRAJECTORIES	C31M	49
C	CORRECTIONS AND IN TRUNCATION ERROR ESTIMATION.	C31M	50
C	FMAF - CUMULATIVE FRACTIONAL MASS AIRBORNE	C31M	51
C	FMBEL - MIN. PARCEL FRACTIONAL MASS ALOFT TO BE TRANSPORTED	C31M	52
C	ICF - MAX. FORMAL DIM. CORRESPONDING TO ICX	C31M	53
C	ICX - OBJECT-TIME FIRST MAX. DIM. OF ARRAY NET. NUMBER OF NET	C31M	54
C	MESHS IN EAST-WEST ROW.	C31M	55
C	IPARIN - LOGICAL UNIT NUMBER OF CR-TRANS. INTER. MOD. OUTPUT TAPE	C31M	56
C	IPOLT - LOGICAL UNIT NUMBER OF DIFF. TRANS. MOD. OUTPUT TAPE	C31M	57
C	ISIN - LOGICAL UNIT NUMBER OF SYSTEM INPUT TAPE	C31M	58

C	ISOUT	- LOGICAL UNIT NUMBER OF SYSTEM OUTPUT TAPE	C31M	59
C	JCF	- MAX. FORMAL DIM. CORRESPONDING TO JCX	C31M	60
C	JCX	- OBJECT-TIME SECOND MAX. DIM. OF ARRAY NET. NUMBER OF NET	C31M	61
C		MESHES IN SOUTH-NORTH ROW.	C31M	62
C	KBH	- ATMOS. VERT. SPACE INDEX FOR ARRAYS USUM,VSUM,WFZ,DXSUM,	C31M	63
C		DYSUM, DFZ, RSUM, ZBH, ZCH	C31M	64
C	KBHF	- MAX. FORMAL DIM. CORRESPONDING TO KBHX	C31M	65
C	KBHX	- OBJECT-TIME MAX. VALUE OF KBH	C31M	66
C	KKF	- MAX. FORMAL DIM. CORRESPONDING TO KKX	C31M	67
C	KKM	- ALWAYS EQUALS 2. CORRESPONDS TO K=0 ALTITUDE INCREMENT	C31M	68
C	KKMA1	- EQUALS KKM+1	C31M	69
C	KKX	- EQUALS KX+KKM	C31M	70
C	KKXS1	- EQUALS KKX-1	C31M	71
C	KPIP	- CONTROL VARIABLE	C31M	72
C		0 FOR ADVECTIVE TRANSPORT	C31M	73
C		1 FOR DIFFUSIVE TRANSPORT	C31M	74
C	KTOPO	- NET MESH AND SUR-MESH TOPOGRAPHY TABLE DATA VECTOR	C31M	75
C	KX	- MAX. NUMBER OF DZ ALTITUDE INCREMENTS	C31M	76
C	KXMIN	- MIN. NUMBER OF DZ ALTITUDE INCREMENTS	C31M	77
C	LSTEP	- NUMBER OF IMPLICIT METHOD ITERATIONS. $\tau_{DELT}=LSTEP*DT$.	C31M	78
C		DYSUM, DFZ, RSUM, TIMUP, DAVG, HAVG	C31M	79
C	LTIM	- ATMOS. UPDATE TIME INDEX FOR ARRAYS USUM,VSUM,WFZ,DXSUM,	C31M	80
C	LTIMX	- OBJECT-TIME MAX. VALUE OF LTIM	C31M	81
C	LTIMF	- MAX. FORMAL DIM. CORRESPONDING TO LTIMX	C31M	82
C	MARF	- MAX. FORMAL DIM. CORRESPONDING TO MARX	C31M	83
C	MARX	- OBJECT-TIME MAX. DIM. OF ARRAY MARY	C31M	84
C	MARY	- HORIZ. ATMOS. SPACE RESOLUTION NET MESH AND SUB-MESH	C31M	85
C		CONTROL FLAGS DATA VECTOR	C31M	86
C			C31M	87
C	MC	- CONTROL INTEGER DATA VECTOR	C31M	88
C			C31M	89
C		MC(1) LESS THAN OR EQUAL TO ZERO, SUPPRESSES LISTING OF	C31M	90
C		EXPANDED WIND AND TURB. DATA	C31M	91
C			C31M	92
C		MC(1) GREATER THAN OR EQUAL TO ONE, CAUSES LISTING OF	C31M	93
C		WIND AND TURB. DATA BEFORE SUMMATION	C31M	94
C			C31M	95
C		MC(1) EQUALS TWO, CAUSES LISTING OF WIND AND TURB. DATA	C31M	96
C		AFTER SUMMATION	C31M	97
C			C31M	98
C		MC(2) EQUALS ONE, SUPPRESSES LISTING OF ATMOS. VISC. AND	C31M	99
C		DENS. TABLES	C31M	100
C			C31M	101
C		MC(3) EQUALS ZERO, SUPPRESSES LISTING OF DEPOSIT	C31M	102
C		INCREMENTS ON TAPE ISOUT	C31M	103
C			C31M	104
C		MC(4) EQUALS ONE, CAUSES PRINTOUT OF TRANSPORT	C31M	105
C		INTERMEDIATE RESULTS ON TAPE ISOUT. WARNING. PRINTOUT	C31M	106
C		IS EXTRAORDINARILY VOLUMINOUS. FOR DEBUGGING ONLY.	C31M	107
C			C31M	108
C		MC(7) EQUALS ONE, SUPPRESSES LISTING OF RAW WIND AND TURB.	C31M	109
C		INPUT DATA	C31M	110
C			C31M	111
C		MC(10) EQUALS ONE, CAUSES TURB. DATA TO BE TREATED AS	C31M	112
C		KOLMOGOROFF-BATCHELOR ENERGY DISSIPATION RATES	C31M	113
C			C31M	114
C		MC(10) NOT EQUAL TO ONE, CAUSES TURB. DATA TO BE TREATED	C31M	115
C		AS FICKIAN DIFFUSIVITIES	C31M	116

C			C31M 117
C		MC(18) EQUALS ONE, SUPPRESSES READING FROM TAPE IPARIN	C31M 118
C		AND WRITING CINTO TAPE IPOUT	C31M 119
C			C31M 120
C	MINT	- MIN. NUMBER OF DT SMALL TIME STEPS PER DEPOSIT INCREMENT	C31M 121
C		TIME INTERVAL	C31M 122
C	NAT	- NUMBER OF ALTITUDE STRATA IN ATMOS. DENS. AND VISC. TABLE	C31M 123
C	NATF	- MAX. FORMAL DIM. CORRESPONDING TO NATF	C31M 124
C	NBLK	- RECORD BLOCK SIZE FOR DEPOSIT INCREMENT RECORDS	C31M 125
C	NCF	- MAX. FORMAL DIM. CORRESPONDING TO NCX	C31M 126
C	NCX	- OBJECT-TIME MAX. DIM. OF ARRAY NETSU	C31M 127
C	NDATA	- ATMOS. HORIZ. SPACE INDEX FOR APRAYS USUM,VSUM,WFZ,DXSUM,	C31M 128
C		DYSUM, DFZ, RSUM, KTOPO	C31M 129
C	NDATC	- HORIZONTAL INDEX OF LATTICE CELL CONTAINING POINT (XC,YC)	C31M 130
C	NDATO	- HORIZONTAL INDEX OF LATTICE CELL CONTAINING POINT (XO,YO)	C31M 131
C	NDATP	- HORIZONTAL INDEX OF LATTICE CELL CONTAINING POINT (XP,YP)	C31M 132
C	NDATX	- OBJECT-TIME MAX. VALUE OF NDATA	C31M 133
C	NDATF	- MAX. FORMAL DIM. CORRESPONDING TO NDATX	C31M 134
C	NDELT	- NOMINAL NUMBER OF DEPOSIT INCREMENTS PER FALLOUT PARCEL	C31M 135
C	NET	- HORIZONTAL SPACE CONTROL NET MESH 2-DIM. ARRAY	C31M 136
C	NETSU	- HORIZONTAL SPACE CONTROL NET SUB-MESH DATA VECTOR	C31M 137
C	NSEQC	- STORAGE SEQUENCE ORDINAL OF FIRST PARCEL TO BE TRANSPORTED	C31M 138
C	PHI	- EQUALS 1-THETA	C31M 139
C	Q(K)	- CONCENTRATION IN K-TH ALTITUDE INCREMENT	C31M 140
C	RHO	- ATMOS. DENSITY DATA VECTOR FOR ATMOS. TABLE	C31M 141
C	RO	- WIND HEADING ORIENTATION ANGLE AFTER ADVECTION	C31M 142
C	ROPART	- FALLOUT PARTICLE DENSITY	C31M 143
C	RSUM	- WIND HEADING ORIENTATION ANGLE (WEIGHTED SUM) 3-DIM. ARRAY	C31M 144
C	RWAF	- PARCEL RADII IN PARCEL CENTRAL PLANE BEFORE ADVECTION	C31M 145
C	SIGXG	- PARCEL MASS HOR. STAND. DEV. DOWNWIND AFTER ADVECTION	C31M 146
C	SIGYG	- PARCEL MASS HOR. STAND. DEV. CROSSWIND AFTER ADVECTION	C31M 147
C	S1	- EQUALS DT/DZ	C31M 148
C	S2	- EQUALS DT/(2*(DZ)**2)	C31M 149
C	TDELT	- CURRENT DEPOSIT INCREMENT TIME INTERVAL	C31M 150
C	TDEP	- ADVECTIVE TRANSPORT TIME INTERVAL	C31M 151
C	THETA	- IMPLICIT FINITE DIFFERENCE PARAMETER	C31M 152
C	THETO	- DOUBLE PRECISION WORD CORRESPONDING TO THETA	C31M 153
C	TIME	- TIME AT ONSET OF CURRENT DEPOSIT INCREMENT TIME INTERVAL	C31M 154
C	TIMEX	- SIMULATED TRANSPORT TIME LIMIT	C31M 155
C	TIMUP	- ATMOSPHERE UPDATE TIMETABLE DATA VECTOR	C31M 156
C	TO	- TIME AFTER PARCEL ADVECTION	C31M 157
C	TP	- TIME BEFORE PARCEL ADVECTION	C31M 158
C	TPAUS	- TIME AT END OF CURRENT DEPOSIT INCREMENT TIME INTERVAL	C31M 159
C	USUM	- WIND X COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY	C31M 160
C	VEFA	- VERTICAL DIFFUSION ABSORPTION COEFFICIENT	C31M 161
C	VSUM	- WIND Y COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY	C31M 162
C	W(K)	- SETTLING RATE AT K-TH SMALL ALTITUDE INCREMENT	C31M 163
C	WAVG	- AVG. ATMOS. VEPT. WIND PER UPDATE PER STRATUM	C31M 164
C	WAVGK	- WAVE AVERAGED OVER THE STRATA FOR THE FIRST UPDATE	C31M 165
C	WFZ	- WIND Z COMPONENT 3-DIM. DATA ARRAY	C31M 166
C	WINT	- NET CONTROL MESH DIMENSION	C31M 167
C	XLLC	- X COORDINATE OF SOUTH-WEST CORNER OF ATMOS. SPACE	C31M 168
C	XO	- PARCEL CENTER X COORDINATE AFTER ADVECTION	C31M 169
C	XP	- PARCEL CENTER X COORDINATE BEFORE ADVECTION	C31M 170
C	YLLC	- X YCOORDINATE OF SOUTH-WEST CORNER OF ATMOS. SPACE	C31M 171
C	YO	- PARCEL CENTER Y COORDINATE AFTER ADVECTION	C31M 172
C	YP	- PARCEL CENTER Y COORDINATE BEFORE ADVECTION	C31M 173
C	ZBH	- ATMOSPHERE STRATA BASE-ALTITUDE DATA VECTOR	C31M 174

C	ZCH	-	ATMOSPHERE STRATA MID-ALTITUDE DATA VECTOR	C31M	175
C	ZDEP	-	ADVECTIVE TRANSPORT TERMINAL ALTITUDE	C31M	176
C	ZHT(K)	-	K-TH ALTITUDE INCREMENT ABOVE ZMIN LEVEL	C31M	177
C	ZLOW	-	PARCEL BASE ALTITUDE BEFORE ADVECTION	C31M	178
C	ZMAX	-	ATMOSPHERE TOP ALTITUDE (FOR VERT. DIFF. DIFF. EQ.)	C31M	179
C	ZMIN	-	GROUND LEVEL OR DEPOSITION PLANE ALTITUDE	C31M	180
C	ZO	-	PARCEL CENTER Z COORDINATE AFTER ADVECTION	C31M	181
C	ZP	-	PARCEL CENTER Z COORDINATE BEFORE ADVECTION, EXCEPT AS	C31M	182
C			REDEFINED IN SUB. ADVEC	C31M	183
C	ZUPP	-	PARCEL TOP ALTITUDE BEFORE ADVECTION. ZLOW+DWAF	C31M	184
	DOUBLE PRECISION AA(204),BB(204),CC(204),DENOM(204),E(204),F(204)			C31M	185
	DOUBLE PRECISION Q(204)			C31M	186
	DIMENSION ZBH(27),ZCH(27),TIMUP(6),MARY(1)			C31M	187
	DIMENSION KTOPO(1),NETSU(1),NET(1, 1)			C31M	188
	DIMENSION DFZ(27, 1, 6),WFZ(27, 1, 6)			C31M	189
	DIMENSION USUM(27, 1, 6),VSUM(27, 1, 6)			C31M	190
	DIMENSION OXSUM(27, 1, 6),OYSUM(27, 1, 6)			C31M	191
	DIMENSION RSUM(27, 1, 6),DAVG(6)			C31M	192
	DIMENSION WAVG(27, 6)			C31M	193
	DIMENSION ALT(260),RHO(260),ATEMP(260)			C31M	194
	DIMENSION CAVS(27),W(204),DIFF(204),ZHT(204)			C31M	195
	COMMON /QPARM/ IPOUT,IPARIN,NBLK,NAT,NDELT,KX,KKM			C31M	196
	1,NSEQO,ICX,JCX,NCX,KBHX,NDATX,LTIMX,ISIN,ISOUT			C31M	197
	2,EDDY,FHREL,LSFEF,MC(13),WINT,XLLC,YLLC,YHETA,ZMIN			C31M	198
	3,CSKIP,MINT,ZMAX,TIMEX,DT,DZ,XP,YP,ZP			C31M	199
	4,DINCR,DOWN,TP,ZLOW,DWAF,PHAF,ROPART,ZUPP,VETA			C31M	200
	5,DOPEN,CROSS,TIME,KKMA1,KXX,KKXS1,KXMIN,NDATP			C31M	201
	ICF=1			C31M	202
	ISIN=5			C31M	203
	ISOUT=6			C31M	204
	IPARIN=9			C31M	205
	IPOUT=10			C31M	206
	JCF=1			C31M	207
	KBHF=27			C31M	208
	KKF=204			C31M	209
	LTIMF=6			C31M	210
	MARF=1			C31M	211
	NATF=260			C31M	212
	NCF=1			C31M	213
	NDATF=1			C31M	214
	DO 1 N=1,NCF			C31M	215
	1 NETSU(N)=0			C31M	216
	DO 2 J=1,JCF			C31M	217
	DO 2 I=1,ICF			C31M	218
	2 NET(I,J)=0			C31M	219
	DO 3 M=1,MARF			C31M	220
	3 MARY(M)=0			C31M	221
	DO 4 K=1,KBHF			C31M	222
	ZBH(K)=0.			C31M	223
	4 ZCH(K)=0.			C31M	224
	DO 104 K=1,KBHF			C31M	225
	DO 104 L=1,LTIMF			C31M	226
	104 WAVG(K,L)=0.0			C31M	227
	DO 5 N=1,NDATF			C31M	228
	5 KTOPO(N)=0			C31M	229
	DO 6 L=1,LTIMF			C31M	230
	TIMUP(L)=0.			C31M	231
	DAVG(L)=0.			C31M	232

DO 6 N=1,NDATE	C31M 233
DO 6 K=1,KRHF	C31M 234
DFZ(K,N,L)=0.	C31M 235
WFZ(K,N,L)=0.	C31M 236
USUM(K,N,L)=0.	C31M 237
VSUM(K,N,L)=0.	C31M 238
DXSUM(K,N,L)=0.	C31M 239
DYSUM(K,N,L)=0.	C31M 240
6 RSUM(K,N,L)=0.	C31M 241
COMMENCE READING DATA INPUTS FROM TAPES ISIN AND IPARIN	C31M 242
COMMENCE WRITING DATA OUTPUT HEADERS ONTO TAPES ISOUT AND IPOUT	C31M 243
CALL LINK(ALT,RHO,ATEMP,NATF)	C31M 244
CONSTRUCT THE HORIZONTAL SPACE CONTROL NET	C31M 245
CALL GETUP(NET,NETSU,KTOPC,MARY,MARF,ICF,JCF,NCF,NDATE)	C31M 246
CONSTRUCT THE ATMOSPHERIC STRATA AND UPDATE DATA VECTORS	C31M 247
CALL HITIME(ZCH,ZOH,TIMUP,KRHF,LTIME)	C31M 248
CONSTRUCT AND FILL IN THE ATMOSPHERIC LATTICE AND UPDATE STRUCTURE	C31M 249
CALL ADMIN(NET,NETSU,ZRH,ZCH,TIMUP,USUM,VSUM,DXSUM,DYSUM,	C31M 250
1RSUM,DFZ,WFZ,DAVG,WAVG,ICF,JCF,NCF,KRHF,NDATE,LTIME)	C31M 251
CIRCUMVENT ALL TAPE HANDLING IF MC(18) EQUALS 1	C31M 252
IF(MC(18).EQ.1) GO TO 7	C31M 253
CALCULATE THE DIFFUSIVE TRANSPORT OF PARCELS ACCEPTED FROM TAPE IPARIN	C31M 254
COPY OUT RESULTS ONTO TAPE IPOUT	C31M 255
CALL SPRVS(NET,NETSU,ZRH,ZCH,TIMUP,USUM,VSUM,DXSUM,DYSUM,	C31M 256
1RSUM,DFZ,WFZ,DAVG,WAVG,ALT,RHO,ATEMP,AA,BB,CC,DENOM,DIFF,E,F,G,W,	C31M 257
2ZHT,ICF,JCF,NCF,KRHF,NDATE,LTIME,KKF,NATF,CAVS)	C31M 258
7 CALL EXIT	C31M 259
STOP	C31M 260
END	C31M 261

SUBROUTINE ADMIN(NET,NETSU,ZBH,ZCH,TIMUP,USUM,VSUM,DXSUM,DYSUM,	ADMIN	1
1RSUM,DFZ,WFZ,DAVG,WAVG,ICF,JCF,NCF,KBHF,NOATF,LTIMF)	ADMIN	2
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SURROUTINE ADMIN CONSTRUCTS WIND DATA ARRAYS	ADMIN	4
USUM, VSUM, WFZ, WAVG, RSUM	ADMIN	5
AND TURBULENCE DATA ARRAYS	ADMIN	6
DXSUM, DYSUM, DFZ, DAVG.	ADMIN	7
IN ADMIN ONLY LTIM AND SPEC ARE READ FROM TAPE ISIN.	ADMIN	8
SPEC - DATA SPECIES IDENTIFICATION WORD #WIND# OR #SPEC#	ADMIN	9
LTIM - UPDATE ORDINAL OF DATA SET. FIRST ATMOS. SET HAS LTIM=1.	ADMIN	10
SUB. MKDAT IS CALLED TO PERFORM DATA EXTRAPOLATIONS.	ADMIN	11
AREA - AREA OF HORIZ. SPACE NET	ADMIN	12
AREAN - AREA OF N-TT NET MESH OR SUB-MESH	ADMIN	13
COMMON /OPARM/ IPOUT,IPARIN,NBLK,NAT,NDELT,KX,KKM	ADMIN	14
1,NSEQD,ICX,JCX,NCX,KBHX,NOATX,LTIMX,ISIN,ISOUT	ADMIN	15
2,FDDY,FMBEL,LSTEP,MC(18),WINT,XLLC,YLLC,THETA,ZMIN	ADMIN	16
3,CSKIP,MINT,ZMAX,TIMEX,DT,DZ,XP,YP,ZP	ADMIN	17
4,OTINCR,DOWH,TP,ZLOW,DWAF,RWAF,ROPART,ZUPP,VETA	ADMIN	18
5,DOOPEN,CROSS,TIME,KKMA1,KKX,KKXS1,KXMIN,NOATP	ADMIN	19
DIMENSION RSUM(KBHF,NOATF,LTIMF),DAVG(LTIMF),WAVG(KBHF,LTIMF)	ADMIN	20
DIMENSION NET(ICF,JCF),NETSU(NCF),ZCH(KBHF),TIMUP(LTIMF),ZBH(KBHF)	ADMIN	21
DIMENSION USUM(KBHF,NOATF,LTIMF),VSUM(KBHF,NOATF,LTIMF)	ADMIN	22
DIMENSION DXSUM(KBHF,NOATF,LTIMF),DYSUM(KBHF,NOATF,LTIMF)	ADMIN	23
DIMENSION DFZ(KBHF,NOATF,LTIMF),WFZ(KBHF,NOATF,LTIMF)	ADMIN	24
DIMENSION LW(10),LD(10)	ADMIN	25
INTEGER WIND,DFSN,DCNE,SPEC	ADMIN	26
DATA PROGRAM/#ADMIN #/	ADMIN	27
DATA WIND/#WIND#/	ADMIN	28
DATA DFSN/#DIFF#/	ADMIN	29
DATA DONE/#NO M#/	ADMIN	30
1 FORMAT(#0#36X,#UPDATE TIME INDEX#I5,#. WIND GRID CELL INDEX#I5/)	ADMIN	31
2 FORMAT(# WIND#2(6X,#HORIZONTAL#),6X,# VERTICAL #6X,#CROSSWIND #6X	ADMIN	32
1,# DOWNWIND #6X,# VERTICAL #6X,#HORIZONTAL#)	ADMIN	33
3 FORMAT(# LAYER#6X,#E.-W. WIND#6X,#N.-S. WIND#6X,# WIND #3(6X,#	ADMIN	34
2DIFFUSION #),6X,# ROTATION#)	ADMIN	35
4 FORMAT(# INDEX#3(6X,# VELOCITY #),3(6X,# CONSTANT #),6X,# ANGLE#)	ADMIN	36
5 FORMAT(# #I5,7E16.4)	ADMIN	37
6 FORMAT(/25X,#WEIGHTED SUMS OVER ABOVE COLUMN ENTRIES#)	ADMIN	38
7 FORMAT(# #I5,2E16.4,16X,2E16.4,16X,E16.4)	ADMIN	39
8 FORMAT(# #22X,#UPDATE#I4,#* CELL#I4,	ADMIN	40
9AVG. VERT. DIFF. =#E12.4)	ADMIN	41
9 FORMAT(36X,I2,8X,3A4)	ADMIN	42
10 FORMAT(/25X,#ATMOSPHERE UPDATE#I4,# FOR TIMES LATER THAN #E12.4,#	ADMIN	43
1SECONDS#)	ADMIN	44
11 FORMAT(# #25X,#* * * * * WINDFIELD EXTRAPOLATION * * *	ADMIN	45
1 * * * * * #/)	ADMIN	46
12 FORMAT(# #25X,#* * * * * DIFFUSIVITY EXTRAPOLATION * * *	ADMIN	47
2 * * * * * #/)	ADMIN	48
13 FORMAT(/25X,#UPDATE#I4,# OF THE WINDFIELD IS MISSING#)	ADMIN	49
14 FORMAT(/25X,#UPDATE#I4,# OF THE DIFFUSIVITY IS MISSING#)	ADMIN	50
15 FORMAT(# OVER ENTIRE HORIZONTAL GRID FOR UPDATE#I4,	ADMIN	51
6 * * AVG. VERT. DIFF. =#E12.4)	ADMIN	52
16 FORMAT(# AVG. VERT. VEL. FOR EACH STRATUM IS - #)	ADMIN	53
17 FORMAT(2X,I5,E16.4)	ADMIN	54
AREA=ICX*JCX*(WINT**2)	ADMIN	55
DO 999 L=1,LTIMX	ADMIN	56
LW(L)=L	ADMIN	57
	ADMIN	58

999 LD(L)=L	ADMIN 59
COPY IN LTIM AND SPEC FROM TAPE ISIN AND CALL SUB. MKDAT	ADMIN 60
1000 READ(ISIN,9) LTIM,SPEC	ADMIN 61
IF(SPEC.EQ.DCNE) GO TO 1301	ADMIN 62
IF((LTIM.LT.1).OR.(LTIM.GT.LTIMX)) CALL ERROR(PROGRM,-1000,ISOUT)	ADMIN 63
WRITE(ISOUT,10) LTIM,TIMUP(LTIM)	ADMIN 64
IF(SPEC.EQ.WIND) GO TO 1101	ADMIN 65
IF(SPEC.EQ.DFSN) GO TO 1201	ADMIN 66
CALL ERROR(PROGRM,-1101,ISOUT)	ADMIN 67
1101 WRITE(ISOUT,11)	ADMIN 68
DO 1102 L=1,LTIMX	ADMIN 69
1102 IF(LTIM.EQ.LW(L)) GO TO 1103	ADMIN 70
CALL ERROR(PROGRM,-1102,ISOUT)	ADMIN 71
1103 LW(L)=-1	ADMIN 72
CALL MKDAT(ZCH,NET,NETSU,LTIM, USUM, VSUM,WFZ,ICF,JCF,NCF,	ADMIN 73
1KBHF,NOATF,LTIMF)	ADMIN 74
GO TO 1000	ADMIN 75
1201 WRITE(ISOUT,12)	ADMIN 76
DO 1202 L=1,LTIMX	ADMIN 77
1202 IF(LTIM.EQ.LD(L)) GO TO 1203	ADMIN 78
CALL ERROR(PROGRM,-1202,ISOUT)	ADMIN 79
1203 LD(L)=-1	ADMIN 80
CALL MKDAT(ZCH,NET,NETSU,LTIM,DXSUM,DYSUM,DFZ,ICF,JCF,NCF,	ADMIN 81
1KBHF,NOATF,LTIMF)	ADMIN 82
GO TO 1000	ADMIN 83
CHECK IF ANY WIND DATA SETS ARE MISSING	ADMIN 84
1301 DO 1303 L=1,LTIMX	ADMIN 85
IF(LW(L).EQ.-1) GO TO 1302	ADMIN 86
WRITE(ISOUT,13) LTIM	ADMIN 87
CALL ERROR(PROGRM,-1302,ISOUT)	ADMIN 88
CHECK IF ANY TURBULENCE DATA SETS ARE MISSING	ADMIN 89
1302 IF(LD(L).EQ.-1) GO TO 1303	ADMIN 90
WRITE(ISOUT,14) LTIM	ADMIN 91
CALL ERROR(PROGRM,-1303,ISOUT)	ADMIN 92
1303 CONTINUE	ADMIN 93
CALCULATE THE WEIGHTED SUMS OVER ATMOS. STRATA AND REWRITE ARRAYS	ADMIN 94
C USUM, VSUM, RSUM, DXSYM, DYSUM. ALSO COMPUTE DAVG AND WAVG.	ADMIN 95
ZSPAN=ZBH(KBHX)-ZBH(1)	ADMIN 96
DO 922 L=1,LTIMX	ADMIN 97
DO 1304 LK=1,KBHX	ADMIN 98
1304 WAVG(LK,L)=0.0	ADMIN 99
DAVG(L)=0.	ADMIN100
DO 921 N=1,NOATX	ADMIN101
DKAV=0.	ADMIN102
IF(MC(1).LT.1) GO TO 915	ADMIN103
WRITE(ISOUT,1) L,N	ADMIN104
WRITE(ISOUT,2)	ADMIN105
WRITE(ISOUT,3)	ADMIN106
WRITE(ISOUT,4)	ADMIN107
915 DO 920 K=1,KBHX	ADMIN108
UKNL=USUM(K,N,L)	ADMIN109
VKNL=VSUM(K,N,L)	ADMIN110
IF(ABS(UKNL)-1.0E-30) 9151,9154,9154	ADMIN111
9151 IF(ABS(VKNL)-1.0E-30) 9152,9153,9153	ADMIN112
9152 RKNL=0.	ADMIN113
GO TO 9155	ADMIN114
9153 RKNL=1.57079633	ADMIN115
GO TO 9155	ADMIN116

9154	RKNL=ATAN(VKNL/UKNL)	ADMIN117
9155	DXKNL=DXSUM(K,N,L)	ADMIN118
	DYKNL=DYSUM(K,N,L)	ADMIN119
	IF(K-KBHX) 916,9156,920	ADMIN120
9156	RSUM(K,N,L)=RKNL	ADMIN121
	GO TO 9195	ADMIN122
916	ZSTEP=ZBH(K+1)-ZBH(K)	ADMIN123
	USUM(K,N,L)=UKNL*ZSTEP	ADMIN124
	VSUM(K,N,L)=VKNL*ZSTEP	ADMIN125
	RSUM(K,N,L)=RKNL*ZSTEP	ADMIN126
	DXSUM(K,N,L)=DXKNL*ZSTEP	ADMIN127
	DYSUM(K,N,L)=DYKNL*ZSTEP	ADMIN128
	DSUM=ZSTEP*DFZ(K,N,L)	ADMIN129
	M=K-1	ADMIN130
	IF(M) 920,919,918	ADMIN131
918	USUM(K,N,L)=USUM(K,N,L)+USUM(M,N,L)	ADMIN132
	VSUM(K,N,L)=VSUM(K,N,L)+VSUM(M,N,L)	ADMIN133
	RSUM(K,N,L)=RSUM(K,N,L)+RSUM(M,N,L)	ADMIN134
	DXSUM(K,N,L)=DXSUM(K,N,L)+DXSUM(M,N,L)	ADMIN135
	DYSUM(K,N,L)=DYSUM(K,N,L)+DYSUM(M,N,L)	ADMIN136
919	DKAV=DKAV+DSUM	ADMIN137
9195	IF(MC(1).LT.1) GO TO 920	ADMIN138
	WRITE(ISOUT,5) K,UKNL,VKNL,WFZ(K,N,L),DXKNL,DYKNL,DFZ(K,N,L),PKNL	ADMIN139
920	CONTINUE	ADMIN140
	IF(MC(1).NE.2) GO TO 9205	ADMIN141
	WRITE(ISOUT,6)	ADMIN142
	WRITE(ISOUT,7) (K,USUM(K,N,L),VSUM(K,N,L),DXSUM(K,N,L),	ADMIN143
	2DYSUM(K,N,L),RSUM(K,N,L),K=1,KBHX)	ADMIN144
9205	DKAV=DKAV/ZSPAN	ADMIN145
	WRITE(ISOUT,8) L,N, DKAV	ADMIN146
	CALL CNTR(NET,NETSU,N,XG,YG,ICF,JCF,NCF)	ADMIN147
	XQ=XG	ADMIN148
	YQ=YG	ADMIN149
	CALL NEST(NET,NETSU,XQ,YQ,NDATQ,XL,XR,YL,YU,ICF,JCF,NCF)	ADMIN150
	AREAN=(XR-XL)*(YU-YL)	ADMIN151
	DAVG(L)=DAVG(L)+DKAV*AREAN	ADMIN152
	DO 9210 KL=1,KBHX	ADMIN153
9210	HAVG(KL,L)=HAVG(KL,L)+WFZ(KL,N,L)*AREAN	ADMIN154
921	CONTINUE	ADMIN155
	DAVG(L)=DAVG(L)/AREAN	ADMIN156
	DO 9215 KL=1,KBHX	ADMIN157
9215	HAVG(KL,L)=HAVG(KL,L)/AREAN	ADMIN158
	WRITE(ISOUT,15) L, DAVG(L)	ADMIN159
	WRITE(ISOUT,16)	ADMIN160
	WRITE(ISOUT,17) (K,HAVG(K,L),K=1,KBHX)	ADMIN161
922	CONTINUE	ADMIN162
	RETURN	ADMIN163
	END	ADMIN164

	SUBROUTINE ADVEC(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,	ADVEC	1
	1TDEP,CAV,PMAS,PSIZ,ICF,JCF,NCF,KBHF,NDATF,LTIME,CAVS,WFZ)	ADVEC	2
C	SEPTEMBER, 1971	ADVEC	3
C	SUBROUTINE ADVEC TRANSPORTS PARCELS BY SIMPLE ADVECTION PLUS	ADVEC	4
C	SETTLING. PARCEL TOP AND BASE ARE TRANSPORTED SEPARATELY, AND THE	ADVEC	5
C	RESULTS ARE SHEARED. THE COMMON VARIABLE ZP IS REDEFINED HEREIN.	ADVEC	6
C	ZP - PARCEL CENTER Z COORDINATE BEFORE ADVECTION, EXCEPT AS	ADVEC	7
C	REDEFINED IN SUB. ADVEC	ADVEC	8
	COMMON /QPARM/ IPOUT ,IPARIN,NBLK ,NAT ,NDEL ,KX ,KKH	ADVEC	9
	1,NSEQO ,ICX ,JCX ,NCX ,KBHX ,NDATX ,LTIMX ,ISIN ,ISOUT	ADVEC	10
	2,EDDY ,FMBEL ,LSTEP ,MC(18),WINT ,XLLC ,YLLC ,THETA ,ZMIN	ADVEC	11
	3,CSKIP ,MINT ,ZMAX ,TIMEX ,DT ,DZ ,XP ,YP ,ZP	ADVEC	12
	4,DINCR ,DOWN ,TP ,ZLOW ,DWAFF ,RWAFF ,ROPART,ZUPP ,VETA	ADVEC	13
	5,DOPEN ,CROSS ,TIME ,KKMA1 ,KKX ,KKXS1 ,KXMIN ,NDATP	ADVEC	14
	DIMENSION NET(ICF,JCF),NETSU(NCF),ZBH(KBHF),USUM(KBHF,NDATF,LTIME)	ADVEC	15
	DIMENSION VSUM(KBHF,NDATF,LTIME),DXSUM(KBHF,NDATF,LTIME)	ADVEC	16
	DIMENSION DYSUM(KBHF,NDATF,LTIME),TIMUP(LTIME)	ADVEC	17
	DIMENSION RSUM(KBHF,NDATF,LTIME)	ADVEC	18
	DIMENSION CAVS(KBHF,WFZ(KBHF,NDATF,LTIME)	ADVEC	19
	MC3=MC(3)	ADVEC	20
	EPS=0.1	ADVEC	21
	NDEP=0	ADVEC	22
	ZDEP=ZMIN	ADVEC	23
	CHANGE ZP FROM PARCEL CENTER TO PARCEL BASE ALTITUDE.	ADVEC	24
	ZP=ZLOW	ADVEC	25
	CALCULATE TRANSPORT OF PARCEL BASE.	ADVEC	26
	IF ((ZP-ZDEP).LE.EPS) GO TO 1411	ADVEC	27
	CALL TRANP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,PSUM,	ADVEC	28
	1NDEP,TDEP,ZDEP,XOL,YOL,ZOL,TOL,SIGXL,SIGYL,ROL,NDATL,ICF,JCF,NCF,	ADVEC	29
	2KBHF,NDATF,LTIME,0,CAVS,WFZ)	ADVEC	30
	GO TO 1412	ADVEC	31
1411	TOL=TP	ADVEC	32
	XOL=XP	ADVEC	33
	YOL=YP	ADVEC	34
	ZOL=ZP	ADVEC	35
	ROL=0.	ADVEC	36
	SIGXL=RWAFF	ADVEC	37
	SIGYL=RWAFF	ADVEC	38
	CHANGE ZP FROM PARCEL BASE TO PARCEL TOP ALTITUDE.	ADVEC	39
	1412 ZP=ZLOW+DWAFF	ADVEC	40
	CALCULATE TRANSPORT OF PARCEL TOP.	ADVEC	41
	IF(ZP-ZDEP .LE.EPS) GO TO 1414	ADVEC	42
	CALL TRANP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,	ADVEC	43
	1NDEP,TDEP,ZDEP,XOU,YOU,ZOU,TOU,SIGXU,SIGYU,ROU,NDATU,ICF,JCF,NCF,	ADVEC	44
	2KBHF,NDATF,LTIME,0,CAVS,WFZ)	ADVEC	45
	GO TO 1415	ADVEC	46
1414	TOU=TP	ADVEC	47
	XOU=XP	ADVEC	48
	YOU=YP	ADVEC	49
	ZOU=ZP	ADVEC	50
	ROU=0.	ADVEC	51
	SIGXU=RWAFF	ADVEC	52
	SIGYU=RWAFF	ADVEC	53
	CALCULATE SHEAR OF PARCEL TOP AND BASE RESULTS.	ADVEC	54
	1415 ZOUTN=(ZOL+ZOU)/2.	ADVEC	55
	TOUTN=(TOL+TOU)/2.	ADVEC	56
	IF(ABS(XOU-XOL).GE.1.0E-30) GO TO 1404	ADVEC	57
	IF(ABS(YOU-YOL).GE.1.0E-30) GO TO 1403	ADVEC	58

ROUTN=0.	ADVEC 59
GO TO 1405	ADVEC 60
1403 ROUTN=1.57079633	ADVEC 61
GO TO 1405	ADVEC 62
1404 ROUTN=ATAN((YOU-YOL)/(XOU-XOL))	ADVEC 63
1405 R=ROUTN-ROL	ADVEC 64
SXL=1./SQRT((COS(R)/SIGXL)**2+(SIN(R)/SIGYL)**2)	ADVEC 65
SYL=1./SQRT((SIN(R)/SIGXL)**2+(COS(R)/SIGYL)**2)	ADVEC 66
R=ROUTN-ROU	ADVEC 67
SXU=1./SQRT((COS(R)/SIGXU)**2+(SIN(R)/SIGYU)**2)	ADVEC 68
SYU=1./SQRT((SIN(R)/SIGXU)**2+(COS(R)/SIGYU)**2)	ADVEC 69
SXOTN=(SXU+SXL*SQR((XOU-XOL)**2+(YOU-YOL)**2))/2.	ADVEC 70
SYOTN=SQR((SYU*SYL)	ADVEC 71
XOUTN=XOL+(SXOTN-SXL)*COS(ROUTN)	ADVEC 72
YOUTN=YOL+(SXOTN-SXL)*SIN(ROUTN)	ADVEC 73
CALL DUMPER(XOUTN,YOUTN,ZOUTN,TOUTN,SXOTN,SYOTN,PHAS,PSIZ,ROUTN,0,	ADVEC 74
1ISOUT,IPOUT,MC3,NBLK)	ADVEC 75
RETURN	ADVEC 76
END	ADVEC 77

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SURROUTINE AMBNT(ZCH,DFZ,WFZ,ZHT,W,DIFF,AA,BB,CC,DENOM,E,F,NET, AMPNT 1
1NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,NTRIP,LTIM,ICF,JCF,NCF, AMPNT 2
2KBHF,NDATF,LTIMF,KKF,CAVS) AMPNT 3
C SEPTEMBER 1971 AMPNT 4
C SUBROUTINE AMBNT DETERMINES FROM INPUT FALL RATE AND VERTICAL WIND AMPNT 5
C AND TURBULENCE DATA THE COEFFICIENT DATA VECTORS AMPNT 6
C  $AA(K)=S2*(DIFF(K+1)+DIFF(K))+S1*F(K+1),$  AMPNT 7
C  $BB(K)=S2*(DIFF(K+1)+2.*DIFF(K)+DIFF(K-1))+S1*F(K),$  AMPNT 8
C  $CC(K)=S2*(DIFF(K)+DIFF(K-1)),$  AMPNT 9
C  $DENOM(K)=1+THETA*(BB(K)-CC(K)*E(K-1)),$  AMPNT 10
C  $E(K)=THETA*AA(K)/DENOM(K),$  AMPNT 11
C WHERE AMPNT 12
C  $S1=DT/DZ,$  AMPNT 13
C  $S2=DT/(2.*(DZ)**2)),$  AMPNT 14
C AND F IS A TEMPORARY WORKING SPACE FOR VERTICAL VELOCITIES. AMPNT 15
C NOTE THAT Q(K) FOR THE NEXT TIME STEP IS GIVEN BY AMPNT 16
C  $AA(K)*Q(K+1)-BB(K)*Q(K)+CC(K)*Q(K-1).$  AMPNT 17
C DFKXS1- VERTICAL DIFFUSIVITY AT ALTITUDE INCREMENT KX-1 AMPNT 18
C LTIM - ATMOS. UPDATE INDEX FOR ARRAYS DFZ AND WFZ AMPNT 19
C NTRIP - OPTION CODE FOR HORIZONTAL ADVECTION OF MASS ALOFT AMPNT 20
C POSITIVE IF NDATO IS STORED IN NTRIP AMPNT 21
C NEGATIVE IF NDATO IS TO BE FOUND VIA CALL TO SUB. TRANSP AMPNT 22
COMMON /OPARM/ IPOUT,IPARIN,NBLK,NAT,NDDELT,KX,KKM AMPNT 23
1,NSEQO,ICX,JCX,KCX,KBHX,NDATX,LTIMX,ISIN,ISOUT AMPNT 24
2,EDDY,FMBEL,LSTEP,MC(19),WINT,XLLC,YLLC,THETA,ZMIN AMPNT 25
3,CSKIP,MINT,ZMAX,TIMEX,DT,DZ,XP,YP,ZP AMPNT 26
4,DINCR,DOWN,TP,ZLOW,DWAF,PWAF,ROPART,ZUPP,VETA AMPNT 27
5,DOPEN,CROSS,TIME,KKMA1,KKX,KKXS1,KXMIN,NDATP AMPNT 28
COMMON /OORLE/DFKXS1,EFFLUX,FMBAB,PHI,THETO AMPNT 29
DOUBLE PRECISION AA(KKF),BB(KKF),CC(KKF),DENOM(KKF),E(KKF),F(KKF) AMPNT 30
DIMENSION DIFF(KKF),W(KKF),ZHT(KKF),DFZ(KBHF,NDATF,LTIMF) AMPNT 31
DIMENSION WFZ(KBHF,NDATF,LTIMF),TIMUP(LTIMF),ZBH(KBHF),ZCH(KBHF) AMPNT 32
DIMENSION DXSUM(KBHF,NDATF,LTIMF),DYSUM(KBHF,NDATF,LTIMF) AMPNT 33
DIMENSION USUM(KBHF,NDATF,LTIMF),VSUM(KBHF,NDATF,LTIMF) AMPNT 34
DIMENSION RSUM(KBHF,NDATF,LTIMF),NET(ICF,JCF),NETSU(NCF) AMPNT 35
DIMENSION CAVS(KBHF) AMPNT 36
DOUBLE PRECISION DFKXS1,EFFLUX,FMBAB,PHI,THETO AMPNT 37
DOUBLE PRECISION S1,S2 AMPNT 38
DATA PROGRAM//AMBNT// AMPNT 39
CONSTRUCT F AND DIFF FOR K=0,...,KX AMPNT 40
NDEP=100 AMPNT 41
TDEP=TIME AMPNT 42
NDATO=IABS(NTRIP) AMPNT 43
COMPUTE KBH AND INITIALIZE AMPNT 44
DIFF(KKM)=0. AMPNT 45
F(KKM)=0. AMPNT 46
ZOLD=ZHT(KKM) AMPNT 47
DOLD=DIFF(KKM) AMPNT 48
FOLD=F(KKM) AMPNT 49
DO 1 K=1,KBHX AMPNT 50
KBH=K AMPNT 51
ZNEW=ZCH(KBH) AMPNT 52
IF(ZOLD.LT.ZNEW) GO TO 2 AMPNT 53
1 IF(KBH.EQ.KBHX) CALL ERPOP(PPROGM,-1,ISOUT) AMPNT 54
2 IF(NTRIP.LT.-1) AMPNT 55
1CALL TRANSP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM, AMPNT 56
2NDEP,TDEP,ZNEW,ZO,YC,ZC,TO,SIGAO,SIGYO,RO,NDATO,ICF,JCF,NCF,KBHF, AMPNT 57
3NDATF,LTIMF,1,CAVS,WFZ) AMPNT 58

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DNEW=DFZ(KBH,NDATO,LTIM)
FNEW=-WFZ(KBH,NDATO,LTIM)
DSLOPE=(DNEW-DOLD)/(ZNEW-ZOLD)
FSLOPE=(FNEW-FOLD)/(ZNEW-ZOLD)
DO 5 KK=KKMA1,KKX
ZHTKK=ZHT(KK)
IF(ZHTKK.LT.ZNEW) GO TO 4
IF(KBH.LT.KBHX-1) GO TO 3
40 DIFF(KK)=DNEW
F(KK)=FNEW
GO TO 5
3 KBH=KBH+1
IF(ZHTKK.GE.ZCH(KBH)) GO TO 30
DOLD=DNEW
FOLD=FNEW
ZOLD=ZNEW
GO TO 38
30 KBC=KBH+1
IF(KBC.LT.KBHX-1) GO TO 32
KBH=KBC
31 ZNEW=ZCH(KBH)
IF(NTPIP.LT.-1)
1CALL TRANP(NET,NFTSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,
2NDEP,TDEP,ZNEW,XO,YC,ZO,TO,SIGXO,SIGYO,PO,NDATO,ICF,JCF,NCF,KPHF,
3NDATF,LTIMF,1,CAVS,WFZ)
DNEW=DFZ(KBH,NDATO,LTIM)
FNEW=-WFZ(KBH,NDATO,LTIM)
GO TO 40
32 KBHXM1=KBHX-1
DO 35 K=KBC,KBHXM1
KBH=K
IF(ZHTKK.GE.ZCH(KBH)) GO TO 35
ZOLD=ZCH(KBH-1)
IF(NTPIP.LT.-1)
1CALL TRANP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,PSUM,
2NDEP,TDEP,ZOLD,XO,YC,ZO,TO,SIGXO,SIGYO,PO,NDATO,ICF,JCF,NCF,KPHF,
3NDATF,LTIMF,1,CAVS,WFZ)
DOLD=DFZ(KBH-1,NDATO,LTIM)
FOLD=-WFZ(KBH-1,NDATO,LTIM)
GO TO 35
35 CONTINUE
GO TO 31
38 ZNEW=ZCH(KBH)
IF(NTPIP.LT.-1)
1CALL TRANP(NET,NFTSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,
2NDEP,TDEP,ZNEW,XO,YC,ZO,TO,SIGXO,SIGYO,RO,NDATO,ICF,JCF,NCF,KPHF,
3NDATF,LTIMF,1,CAVS,WFZ)
DNEW=DFZ(KBH,NDATO,LTIM)
FNEW=-WFZ(KBH,NDATO,LTIM)
DSLOPE=(DNEW-DOLD)/(ZNEW-ZOLD)
FSLOPE=(FNEW-FOLD)/(ZNEW-ZOLD)
4 DIFF(KK)=DOLD+DSLOPE*(ZHTKK-ZOLD)
F(KK)=FOLD+FSLOPE*(ZHTKK-ZOLD)
5 CONTINUE
CORRECT DIFFUSIVITIES FOR CROSSING TRAJECTORIES EFFECTS
DO 150 KK=KKM,KKX
150 DIFF(KK)=DOWN*DIFF(KK)
COMBINE STILL-AIR FALL RATES WITH VERTICAL WINDS

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AMBNT 59
AMPNT 60
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AMPNT 113
AMPNT 114
AMPNT 115
AMPNT 116

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      DO 250 KK=KKM,KKX
250 F(KK)=F(KK)+W(KK)
      COMPUTE E(0) IN ACCORDANCE WITH REFLECTIVITY CONTROL VARIABLE VETA
      E(KKM)=U.
      IF(VETA.LT.0.) GO TO 17
      WREF=F(KKM+1)
      DREF=(DIFF(KKM)+DIFF(KKM+1))/(2.*DZ)
      E(KKM)=(WREF+DREF)/(VETA+DREF)
      COMPUTE AA,BB,CC,DENOM, AND E FOR K=1,...,KX-1
17 S2=0Z
   S1=DT
   S1=S1/S2
   GZ=S1/(2.*S2)
   DO 18 KK=KKM+1,KKX
18 CC(KK)=S2*(DIFF(KK)+DIFF(KK-1))
   DO 19 KK=KKM,KKXS1
19 AA(KK)=CC(KK+1)+S1*F(KK+1)
   DO 20 KK=KKM+1,KKXS1
   BB(KK)=AA(KK-1)+CC(KK+1)
   DENOM(KK)=1.+THETA*(BB(KK)-CC(KK)*E(KK-1))
20 E(KK)=THETA*AA(KK)/DENOM(KK)
   DKXS1=DIFF(KKXS1)
C      WRITE(ISOUT,2221)
C2221 FORMAT(10CONTENTS OF ARRAYS ZHT, F, DIFF, AA, BB, CC, DENOM, E)
C      WRITE(ISOUT,2222) ZHT
C      WRITE(ISOUT,2222) F
C      WRITE(ISOUT,2222) DIFF
C      WRITE(ISOUT,2222) AA
C      WRITE(ISOUT,2222) BB
C      WRITE(ISOUT,2222) CC
C      WRITE(ISOUT,2222) DENOM
C      WRITE(ISOUT,2222) E
C2222 FORMAT(10*(13E10.2))
      RETURN
      END

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AMPNT117
AMPNT118
AMPNT119
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AMPNT149
AMPNT150
AMPNT151

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SUBROUTINE SPRVS(NET,NETSU,ZBH,ZCH,TIMUP,USUM,VSUM,DXSUM,DYSUM, SPPVS 1
1RSUM,DFZ,WfZ,DAVG,WAVG,ALT,RHO,ATEMP,AA,BB,CC,DENOM,DIFF,E,F,Q,W, SPPVS 2
2ZHT,ICF,JCF,NCF,KBHF,NDATF,LTIMF,KKF,NATF,CAVS) SPPVS 3
C SEPTEMBER 1971 SPPVS 4
C SUBROUTINE SPRVS SUPERVISES DIFFUSIVE AND/OR ADVECTIVE TRANSPORT SPPVS 5
C OF FALLOUT PARCELS LISTED ON TAPE IPARIN. PARCEL PARAMETERS ARE SPPVS 6
C STORED IN ARRAYS XPAR,YPAR,ZPAR,TPAR,PDAM,PSAM,RWFR,DWFR,ZLWF,VWFR SPPVS 7
C ONLY ONE PARCEL IS TRANSPORTED AT A TIME. FOR THIS PARCEL ABOVE SPPVS 8
C ITEMS ARE STORED IN XP,YP,ZP,TP,PSIZ,PMAS,RWAF,DWAF,ZLOW,VWAF. SPPVS 9
C XPAR - X COORDINATE OF PARCEL CENTER DATA VECTOR (AT TIME TPAR) SPPVS 10
C YPAR - Y COORDINATE OF PARCEL CENTER DATA VECTOR (AT TIME TPAR) SPPVS 11
C ZPAR - Z COORDINATE OF PARCEL CENTER DATA VECTOR (AT TIME TPAR) SPPVS 12
C TPAR - TIME OF DEFINITION OF CLOUD PARCEL DATA VECTOR SPPVS 13
C PDAM - MIDPOINT OF PARCEL PARTICLE SIZE CLASS DATA VECTOR SPPVS 14
C PSAM - TOTAL MASS OF PARCEL DATA VECTOR (AT TIME TPAR) SPPVS 15
C RWFR - RADIUS OF PARCEL AT C. O. M. DATA VECTOR (AT TIME TPAR) SPPVS 16
C DWFR - PARCEL THICKNESS DATA VECTOR (AT TIME TPAR) SPPVS 17
C ZLWF - ALTITUDE OF PARCEL BASE DATA VECTOR (AT TIME TPAR) SPPVS 18
C VWFR - PARCEL VOLUME DATA VECTOR (AT TIME TPAR) SPPVS 19
COMMON /QPARM/ IPOUT,IPARIN,NBLK,NAT,NDELT,KX,KKM SPPVS 20
1,NSEQO,YCX,JCX,NCX,KBHX,NDATX,LTIMX,ISIN,ISOUT SPPVS 21
2,EDDY,FMBEL,LSTEF,MC(19),WINT,XLLC,YLLC,THETA,ZMIN SPPVS 22
3,CSKIP,MINT,ZMAX,TIMEX,DT,DZ,XP,YP,ZP SPPVS 23
4,DINCR,DOWN,TP,ZLOW,DWAF,RWAF,ROPART,ZUPP,VETA SPPVS 24
5,DOPEN,CROSS,TIME,KKMA1,KKX,KKXS1,KXMIN,NDATP SPPVS 25
COMMON /QDBLE/DFKXS1,EFFLUX,FMA8,PHI,THETQ SPPVS 26
DOUBLE PRECISION AA(KKF),BB(KKF),CC(KKF),DENOM(KKF),E(KKF),F(KKF) SPPVS 27
DOUBLE PRECISION Q(KKF) SPPVS 28
DIMENSION ALT(NATF),RHO(NATF),ATEMP(NATF) SPPVS 29
DIMENSION NET(ICF,JCF),NETSU(NCF),ZBH(KBHF),ZCH(KBHF),DIFF(KKF) SPPVS 30
DIMENSION USUM(KBHF,NDATF,LTIMF),VSUM(KBHF,NDATF,LTIMF),W(KKF) SPPVS 31
DIMENSION DXSUM(KBHF,NDATF,LTIMF),DYSUM(KBHF,NDATF,LTIMF) SPPVS 32
DIMENSION DFZ(KBHF,NDATF,LTIMF),ZHT(KKF) SPPVS 33
DIMENSION WFZ(KBHF,NDATF,LTIMF),DAVG(LTIMF),WAVG(KBHF,LTIMF) SPPVS 34
DIMENSION TIMUP(LTIMF),RSUM(KBHF,NDATF,LTIMF) SPPVS 35
DIMENSION XPAR(100),YPAR(100),ZPAR(100),TPAR(100),PDAM(100) SPPVS 36
DIMENSION PSAM(100),RWFR(100),DWFR(100),ZLWF(100),VWFR(100) SPPVS 37
DIMENSION CAVS(KBHF) SPPVS 38
DOUBLE PRECISION DFKXS1,EFFLUX,FMA8,PHI,THETQ SPPVS 39
8014 FORMAT(##T102,E12.4,I4) SPPVS 40
8015 FORMAT(##T103,#AIREORNE (ADVCM)#) SPPVS 41
8016 FORMAT(# #I4,3E12.4) SPPVS 42
8017 FORMAT(##T103,#AIREORNE (DIFFN)#) SPPVS 43
8018 FORMAT(##T103,#ADVECTIVE TRNSPT#) SPPVS 44
8019 FORMAT(##T103,#IMPACTED WAFER#) SPPVS 45
8020 FORMAT(##T103,#OUTSIDE WINDGRID#) SPPVS 46
8021 FORMAT(#0#36X,#PARTICLE SIZE CLASS#E12.4,# MICRONS#) SPPVS 47
8022 FORMAT(# #22X,#FALL RATE#E12.4,# METERS/SEC AT ALTITUDE#E12.4,# SPPVS 48
1 METERS#/22X,#UPPER LIMIT INPUT ALTITUDE FOR ADV. TRANSP. IS#E12.4 SPPVS 49
2,# METERS#) SPPVS 50
8024 FORMAT(#0#T2,#NSEQ#I11,#XP#T23,#YP#T35,#ZP#T47,#TP#T58,#PMAS#T70,# SPPVS 51
1RWAF#T92,#ZLOW#T94,#DWAF#T107,#DZ#T115,#KX#/) SPPVS 52
8025 FORMAT(#0NEGATIVE DEPOSIT. WAFER NO.#I4,# AT TIME#E12.4,#. VARIABLE SPPVS 53
SES EFFLUX,FMA8,DEP #2D12.4,E12.4/) SPPVS 54
DATA PROGRAM/#SPPVS #/ SPPVS 55
JF=100 SPPVS 56
KKMA1=KKM+1 SPPVS 57
THETQ=THETA SPPVS 58

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PHI=1.-THETO	SPRVS 59
KXBF=0	SPRVS 60
MC3=MC(3)	SPRVS 61
NSEQ=0	SPRVS 62
PSZBE=-2.0	SPRVS 63
COMPUTE OVERALL AVERAGE VERTICAL VELOCITY FOR THE FIRST UPDATE	SPRVS 64
WAVGK=0.0	SPRVS 65
KBHM1=KBHX-1	SPRVS 66
DO 50 K=1,KBHM1	SPRVS 67
50 WAVGK=WAVGK + WAVG(K,1)*(ZBH(K+1) - ZBH(K))	SPRVS 68
WAVGK=WAVGK/(ZBH(KBHX)-ZBH(1))	SPRVS 69
COMPUTE TIMEX MARGIN FACTOR FOR ADVECTIVE TRANSPORT AIRBORNE TEST	SPRVS 70
IF(NDATX-1)70,70,60	SPRVS 71
60 SLOP=1.1	SPRVS 72
GO TO 90	SPRVS 73
70 SLOP=1.0	SPRVS 74
COMPUTE MINIMUM SMALL ALTITUDE INCREMENT DZMIN	SPRVS 75
80 DZMIN=(ZMAX-ZMIN)/KX	SPRVS 76
CUC IPARIN TAPE AT BEGINNING OF INPUT PARCEL BLOCK	SPRVS 77
100 READ(IPARIN) NP	SPRVS 78
IF(NP.LE.0) GO TO 806	SPRVS 79
IF(NP.GT.1) CALL ERROR(PROGRM,-100,ISOUT)	SPRVS 80
COPY IN A BLOCK OF INPUT PARCEL PARAMETERS FROM TAPE IPARIN	SPRVS 81
READ(IPARIN) (XPAR(J),YPAR(J),ZPAR(J),TPAR(J),PDAM(J),PSAM(J),	SPRVS 82
1RWFR(J),DWFR(J),ZLWF(J),VWFR(J),J=1,NP)	SPRVS 83
COMMENCE PROCESSING BLOCK OF INPUT PARCELS ONE AT A TIME	SPRVS 84
DO 1000 J=1,NP	SPRVS 85
NSEQ=NSEQ+1	SPRVS 86
IF(NSEQ.LT.NSEQ0) GO TO 1000	SPRVS 87
XP=XPAR(J)	SPRVS 88
YP=YPAR(J)	SPRVS 89
ZP=ZPAR(J)	SPRVS 90
TP=TPAR(J)	SPRVS 91
PSIZ=1.0E6*PDAM(J)	SPRVS 92
PMA5=PSAM(J)	SPRVS 93
RWAF=RWFR(J)/2.	SPRVS 94
DWAF=DWFR(J)	SPRVS 95
ZLOW=ZLWF(J)	SPRVS 96
VWAF=VWFR(J)	SPRVS 97
CHECK FOR NEW PARTICLE SIZE CLASS	SPRVS 98
IF(ABS((PSIZ-PSZBE)/PSIZ).LE.1.0E-10) GO TO 103	SPRVS 99
WRITE(ISOUT,8021) PSIZ	SPRVS100
COMPUTE MID-ATMOSPHERE FALL RATE FAV FOR NEW PARTICLE SIZE CLASS	SPRVS101
H=(ZMIN+ZMAX)/2.	SPRVS102
CALL TRPL(H,NAT,ALT,RHO,DEN)	SPRVS103
CALL TRPL(H,NAT,ALT,ATEMP,VIS)	SPRVS104
CALL FALRT(PSIZ,ROPART,H,DEN,VIS,FAV,ISOUT)	SPRVS105
FAV=FAV-WAVGK	SPRVS106
COMPUTE UPPER LIMIT ALTITUDE FOR ADVECTIVE TRANSPORT OF THIS SIZE PART.	SPRVS107
CALL CALIB(ZBH,KBHX,ZMIN,-1,KBHZ)	SPRVS108
CALL TRPL(ZBH(KBHZ),NAT,ALT,ATEMP,VIS)	SPRVS109
CALL TRPL(ZBH(KBHZ),NAT,ALT,RHO,DEN)	SPRVS110
CALL FALRT(PSIZ,ROPART,ZBH(KBHZ),DEN,VIS,CAV,ISOUT)	SPRVS111
TDEP=TP + (ZBH(KBHZ) - ZMIN) / (CAV - WAVG(KBHZ-1,1))	SPRVS112
KBHM1=KBHX-1	SPRVS113
DO 1001 IZ=KBHZ,KBHM1	SPRVS114
CALL TRPL(ZCH(IZ),NAT,ALT,ATEMP,VIS)	SPRVS115
CALL TRPL(ZCH(IZ),NAT,ALT,RHO,DEN)	SPRVS116

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CALLFALRT(PSIZ,ROPART,ZCH(IZ),DEN,VIS,CAV,ISOUT)
TDEP=TDEP + (ZBH(IZ+1) - ZBH(IZ))/(CAV- WAVG(IZ,1))
IF(TDEP.GT.SLOP*TIMEX) GO TO 1002
1001 CONTINUE
ZLIM=5.0E4
GO TO 1003
1002 ZLIM=ZBH(IZ+1)
1003 WRITE(ISOUT,8022) FAV,H,ZLIM
      WRITE(ISOUT,8024)
COMPUTE PARTICLE FALL RATE TABLE FOR EACH ATMOSPHERIC STRATUM WHEN
C A NEW PARTICLE SIZE IS ENCOUNTERED
DO 101 KKZ=1,KBX
CALL TRPL(ZCH(KKZ),NAT,ALT,ATEMP,VIS)
CALL TRPL(ZCH(KKZ),NAT,ALT,RHO,DEN)
101 CALL FALRT(PSIZ,ROPART,ZCH(KKZ),DEN,VIS,CAVS(KKZ),ISOUT)
COMPUTE DIFFUSIVITY CORRECTIONS FOR NEW PARTICLE SIZE CLASS
DOWN=(FAV*EDDY)**2
CROSS=1./SQRT(1.+4.*DOWN)
DOWN=1./SQRT(1.+DOWN)
PSIZE=PSIZ
103 WRITE(ISOUT,8016) NSEQ,XP,YP,ZP,TP,PMAS,RWAF,ZLOW,DWAF
CANCEL PROCESSING OF PARCEL IF IT HAS ALREADY IMPACTED
IF (IFIX(DWAF).GT.0) GO TO 1200
WRITE(ISOUT,8019)
CALL DUMPER(XP,YP,ZP,TP, RWAF, RWAF, PMAS,PSIZ,0.,0,
1ISOUT,IPOUT,M03,NRLK)
GO TO 1000
COMPUTE INDEX OF MESH OR SUB-MESH CONTAINING PARCEL CENTER POSITION
1200 CALL NEST(NET,NETSU,XP,YP,NDATP,XL,XR,YL,YU,ICF,JCF,NCF)
CANCEL PROCESSING OF PARCEL IF IT IS INPUT OUTSIDE ATMOS.
IF(NDATP.GT.0) GO TO 1248
WRITE(ISOUT,8020)
GO TO 1000
COMPUTE AVERAGE FALL RATE CAV
1248 ZUPP=ZLOW+DWAF
ZLO=ZLCW-ZMIN
ZUP=ZUPP-ZMIN
H=ZMIN+ZUP/2.
CALL TRPL(H,NAT,ALT,RHO,DEN)
CALL TRPL(H,NAT,ALT,ATEMP,VIS)
CALL FALRT(PSIZ,ROPART,H,DEN,VIS,CAV,ISOUT)
CANCEL PROCESSING OF PARCEL IF IT WILL REMAIN AIRBORNE BY DIFFUSION
DAV=DOWN*DAVG(1)
CAV=CAV-WAVGK
TFLY=TIMEX-TP
IF(TFLY.LE.0.) GO TO 1249
CALL ESTH(ZUP,CAV,DAV,TFLY,PUP)
CALL ESTH(ZLO,CAV,DAV,TFLY,PLO)
PDEST=1.0-(PUP-PLO)/(ZUP-ZLO)
IF(CSKIP.LE.PDEST) GO TO 1250
1249 WRITE(ISOUT,8017)
GO TO 1000
COMPUTE TRANSPORT BY ADVECTION IF TRUNCATION ERROR IS EXCEEDED
1250 IF(DZMIN.LE.0.2*DAV/FAV) GO TO 1500
CANCEL PROCESSING OF PARCEL IF IT WILL REMAIN AIRBORNE BY ADVECTION
IF(ZLOW.LT.ZLIM) GO TO 1409
WRITE(ISOUT,8015)
GO TO 1000

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SPRVS117
SPRVS118
SPRVS119
SPRVS120
SPRVS121
SPRVS122
SPRVS123
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SPRVS129
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SPRVS169
SPRVS170
SPRVS171
SPRVS172
SPRVS173
SPRVS174

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1409 WRITE(ISOUT,8018)	SPRVS175
CALL ADVEC(NEI,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,	SPPVS176
1TDEP,CAV,PHAS,PSIZ,ICF,JCF,NCF,K3HF,NDATF,LTINF,CAVS,WFZ)	SPRVS177
GO TO 1000	SPRVS178
COMPUTE SMALL ALTITUDE INCREMENT DZ	SPRVS179
1500 DZMAX=0WAF	SPRVS180
1501 IF(DZMAX.GE.DZMIN) GO TO 1502	SPRVS181
DZMAX=2.0*DZMAX	SPRVS182
GO TO 1501	SPRVS183
1502 DZ=0.2*DAV/FAV	SPRVS184
IF(DZ.GT.DZMAX) DZ=DZMAX	SPRVS185
KX=(ZMAX-ZMIN)/DZ+1.	SPRVS186
IF(KX.LT.KXMIN) KX=KXMIN	SPRVS187
DZ=(ZMAX-ZMIN)/KX	SPRVS188
WRITE(ISOUT,8014) DZ,KX	SPRVS189
COMPUTE ALTITUDE INCREMENT AND FALL RATE DATA VECTORS	SPRVS190
IF(KX.EQ.KXBE) GO TO 1305	SPRVS191
KKX=KKM+KX	SPPVS192
KKXS1=KKX-1	SPPVS193
DO 1304 KK=1,KKX	SPRVS194
ZHT(KK)=ZMIN+DZ*(KK-KKM)	SPRVS195
CALL TRPL(ZHT(KK),NAT,ALT,RHO,DEN)	SPRVS196
CALL TRPL(ZHT(KK),NAT,ALT,ATEMP,VIS)	SPRVS197
1304 CALL FALRT(PSIZ,ROFAP,ZHT(KK),DEN,VIS,W(KK),ISOUT)	SPRVS198
KXBE=KX	SPPVS199
COMPOSE INITIAL CONCENTRATION DATA VECTOR	SPRVS200
1305 CALL CONC(ZHT,0,KKF)	SPRVS201
CANCEL PROCESSING OF WAFER IF INITIAL AIRBORNE MASS IS INADEQUATE	SPRVS202
IF(FMA9.LT.1) GO TO 1000	SPRVS203
DEPBE=0.	SPRVS204
NTRIP=NDATP	SPPVS205
COMPUTE FIRST DEPOSIT INCREMENT TIME INTERVAL TDELT	SPRVS206
TDELT=TFLY/NDELT	SPRVS207
TLARG=TDELT	SPRVS208
TAE=4.*ZUP/(3.*CAV)	SPRVS209
IF(TAE.LT.TFLY) TDELT=TAE/NDELT	SPRVS210
TSMAL=MINT*DT	SPRVS211
IF(TDELT.LT.TSMAL) TDELT=TSMAL	SPRVS212
COMMENCE DEPOSIT TIME LOOP	SPRVS213
TIME=TP	SPPVS214
TPAUS=TIME	SPRVS215
LTIM=-1	SPPVS216
NPASS=1	SPPVS217
XOBE=XP	SPRVS218
YOBE=YP	SPRVS219
1 LSTEP=TDELT/DT +1.	SPRVS220
TDELT=LSTEP*DT	SPPVS221
135 TPAUS=TPAUS+TDELT	SPRVS222
COMPUTE DATA SET TIME INDEX LTIM	SPRVS223
CALL CALIS(TIMUP,LTIMX,TIME,+1,LTIMA)	SPRVS224
IF(LTIM.NE.LTIMA) GO TO 3	SPRVS225
IF(ABS(NTRIP)-1) 31,32,31	SPRVS226
3 LTIM=LTIMA	SPRVS227
COMPOSE CONCENTRATION COEFFICIENT DATA ARRAYS	SPRVS228
31 CALL AMBNT(ZCH,DFZ,WFZ,ZHT,W,DIFF,AA,BB,CC,DENOM,E,F,NET,	SPRVS229
1NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,NTRIP,LTIM,ICF,JCF,NCF,	SPRVS230
2K3HF,NDATF,LTINF,KKF,CAVS)	SPRVS231
NTRIP=-NDATX	SPPVS232

COMPUTE NUMBER OF ITERATIONS LSTEP OF SOLUTION TO VERTICAL DIFFUSION	SPRVS237
C DIFFERENCE EQUATION FOR THIS DEPOSIT INCREMENT TIME INTERVAL	SPRVS234
32 IF(LTIM.GE.LTIMX) GO TO 138	SPRVS235
IF(TPAUS.LT.TIMUP(LTIM+1)) GO TO 140	SPRVS236
TPAUS=TIMUP(LTIM+1)	SPRVS237
TDELT=TPAUS-TIME	SPRVS238
LSTEP=TDELT/DT+1.	SPRVS239
TDELT=LSTEP*DT	SPRVS240
138 IF(TPAUS.LT.TIMEX) GO TO 140	SPRVS241
TPAUS=TIMEX	SPRVS242
TDELT=TPAUS-TIME	SPRVS243
LSTEP=TDELT/DT+1.	SPRVS244
TDELT=LSTEP*DT	SPRVS245
IF(LSTEP.LE.0) GO TO 1000	SPRVS246
140 IF(NPASS.NE.1) GO TO 4	SPRVS247
NPASS=2	SPRVS248
TDELT=TDELT	SPRVS249
COMPUTE DEPOSIT INCREMENT FRACTIONAL MASS DEP	SPRVS250
4 CALL GIFFF(Q,AA,BB,CC,DENOM,E,F,DEP,KKF)	SPRVS251
CHECK DEPOSIT INCREMENT FRACTIONAL MASS DEP AGAINST DOPEN	SPRVS252
IF(DEP.GE.-DOPEN*TDELT) GO TO 5	SPRVS253
WRITE(ISOOT,3025) NSEO,TIME,EFFLUX,FMA8,DEP	SPRVS254
5 IF(DEP.GE.DOPEN*TDELT) GO TO 7	SPRVS255
CHECK CUMULATIVE AIRBORNE FRACTIONAL MASS FMA8 AGAINST FMBEL	SPRVS256
IF(SNGL(FMA8).GT.FMBEL) GO TO 135	SPRVS257
GO TO 1000	SPRVS258
COMPARE RATE OF CHANGE OF DEPOSITION RATE DPDP WITH DINCR AND ADJUST	SPRVS259
C NEXT TDELT	SPRVS260
7 DPDP=((DEP/TDELT)-(DEPRE/TDELTB))/TDELT	SPRVS261
IF(DPDP.LT.DINCR) GO TO 10	SPRVS262
TDELTB=TDELT	SPRVS263
TDELT=TDELT/2.	SPRVS264
IF(TDELT.LT.TSMAL) TDELT=TSMAL	SPRVS265
GO TO 13	SPRVS266
10 IF(DPDP.GT.DINCR) GO TO 13	SPRVS267
TDELTB=TDELT	SPRVS268
TDELT=2.*TDELT	SPRVS269
IF(TDELT.GT.TLARG) TDELT=TLARG	SPRVS270
COMPUTE DEPOSIT INCREMENT MASS PMDEP	SPRVS271
13 PMDEP=PMAS*DEP	SPRVS272
DEPRE=DEP	SPRVS273
NDEP=0	SPRVS274
ZDEP=ZMIN	SPRVS275
TDEP=TIME	SPRVS276
COMPUTE DEPOSIT INCREMENT POSITION (XO,YO,ZO) AND HORIZONTAL DISPERSION	SPRVS277
C PARAMETERS (SIGXO,SIGYO,RO) AT TIME=TO	SPRVS278
CALL TRANP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,PSUM,	SPRVS279
1NDEP,TDEP,ZDEP,XO,YO,ZO,TO,SIGXO,SIGYO,RO,NDATO,ICF,JCF,NCF,KBHF,	SPRVS280
2NDATF,LTIME,1,CAVS,W7)	SPRVS281
CONTINUE ON TO NEXT WAFER IF THIS ONE LIES OUTSIDE WINDFIELD	SPRVS282
IF(NDATO.LE.0) GO TO 1000	SPRVS283
COLLECT FINAL RESULTS FOR THIS WAFER AND STORE IN BUFFER DATA VECTORS	SPRVS284
XH=(XO+XOBE)/2.	SPRVS285
YH=(YO+YOBE)/2.	SPRVS286
CALL DUMPER(XH,YH,ZO,TO,SIGXO,SIGYO,PMDEP,PSIZ,RO,0,	SPRVS287
1ISOOT,ISOOT,MC3,MBLK)	SPRVS288
XOBE=XO	SPRVS289
YOBE=YO	SPRVS290

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      IF (TIME+DT.LT.TIMEX) GO TO 1
1000 CONTINUE
      GO TO 100
COPY OUT BUFFER DATA VECTORS. WAFER PROCESSING HAS BEEN COMPLETED
806 CALL      DUMPER(0.,0.,0.,0., 0., 0., 0., 0.,0.,999,
1ISOUT,IPOUT,MC3,NBLK)
      CALL      DUMPER(0.,0.,0.,0., 0., 0., 0., 0.,0.,999,
1ISOUT,IPOUT,MC3,NBLK)
      REWIND IPARIN
      END FILE IPOUT
      REWIND IPOUT
      RETURN
      END

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SPPVS291
SPPVS292
SPPVS293
SPRVS294
SPRVS295
SPRVS296
SPPVS297
SPPVS298
SPRVS299
SPPVS300
SPPVS301
SPPVS302
SPPVS303

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SUBROUTINE TRANP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM, TRANP 1
1NDEP,TDEP,ZDEP,XO,YC,ZC,TO,SIGXO,SIGYO,RO,NDATO,ICF,JCF,NCF,KBHF, TRANP 2
2NDATF,LTIMF,KRIP,CAVS,WFZ) TRANP 3
SEPTEMBER 1971 TRANP 4
SUBROUTINE TRANP DETERMINES (AT AN INPUT TERMINAL ALTITUDE PLANE) TRANP 5
THE WAFER HORIZONTAL CENTER POSITION AND DISPERSION PARAMETERS FORTRANP 6
AN INPUT TRANSPORT FLIGHT TIME TRANP 7
CAVS - PARTICLE FALL RATE TABULATED FOR EACH ALTITUDE STRATUM TRANP 8
DXSUM - TURBULENCE X COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY TRANP 9
DYSUM - TURBULENCE Y COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY TRANP 10
NET - HORIZONTAL SPACE CONTROL NET MESH 2-DIM. ARRAY TRANP 11
NETSU - HORIZONTAL SPACE CONTROL NET SUB-MESH DATA VECTOR TRANP 12
RSUM - WIND HEADING ORIENTATION ANGLE (WEIGHTED SUM) 3-DIM. ARRAYTRANP 13
USUM - WIND X COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY TRANP 14
VSUM - WIND Y COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY TRANP 15
ZBH - ATMOSPHERE STRATA BASE-ALTITUDE DATA VECTOR TRANP 16
MODE - COMPUTATION MODE SWITCH TRANP 17
      0 RAPID COMPUTATION TRANP 18
      1 LAYERWISE COMPUTATION TRANP 19
NDEP - OPTION CONTROL VARIABLE TRANP 20
      ZERO IF SIGXO AND SIGYO ARE TO BE COMPUTED TRANP 21
      NON-ZERO IF SIGXO AND SIGYO ARE NOT TO BE COMPUTED AND TRANP 22
      IF NDATO IS TO BE POSITIVE ALWAYS TRANP 23
TDEP - ADVECTIVE TRANSPORT TIME INTERVAL TRANP 24
KRIP - CONTROL VARIABLE TRANP 25
      0 FOR ADVECTIVE TRANSPORT TRANP 26
      1 FOR DIFFUSIVE TRANSPORT TRANP 27
WFZ - VERTICAL WIND FIELD TRANP 28
ZDEP - ADVECTIVE TRANSPORT TERMINAL ALTITUDE TRANP 29
TO - TIME AFTER PARCEL ADVECTION TRANP 30
XO - PARCEL CENTER X COORDINATE AFTER ADVECTION TRANP 31
YO - PARCEL CENTER Y COORDINATE AFTER ADVECTION TRANP 32
ZO - PARCEL CENTER Z COORDINATE AFTER ADVECTION TRANP 33
SIGXO - PARCEL MASS HOR. STAND. DEV. DOWNWIND AFTER ADVECTION TRANP 34
SIGYO - PARCEL MASS HOR. STAND. DEV. CROSSWIND AFTER ADVECTION TRANP 35
NDATO - HORIZONTAL INDEX OF LATTICE CELL CONTAINING POINT (XC,YC) TRANP 36
RO - WIND HEADING ORIENTATION ANGLE AFTER ADVECTION TRANP 37
COMMON /OPARM/ IPOUT,IPADIN,NBLK,NAT,NDALT,KX,KKM TRANP 38
1,PSEQO,ICX,JCX,NCX,KBHX,NDATX,LTIMX,ISIN,ISOUT TRANP 39
2,EDDY,FMOEL,LSTEP,MC(15),WINT,XLLC,YLLC,THETA,ZMIN TRANP 40
3,CSQJP,MINT,ZMAX,TIMEX,DT,DZ,XP,YP,ZP TRANP 41
4,DINCP,DCWN,TP,ZLOW,DWAF,RWAF,ROPART,ZUPP,VETA TRANP 42
5,DOPEN,CROSS,TIME,KKJA1,KKX,KKXS1,KXMIN,NDATF TRANP 43
DIMENSION NET(ICF,JCF),NETSU(NCF),ZBH(KBHF),USUM(KBHF,NDATF,LTIMF) TRANP 44
DIMENSION VSUM(/BHF,NDATF,LTIMF),DXSUM(KBHF,NDATF,LTIMF) TRANP 45
DIMENSION DYSUM(KBHF,NDATF,LTIMF),TIMUP(LTIMF) TRANP 46
DIMENSION CAVS(KBHF) TRANP 47
DIMENSION RSUM(KBHF,NDATF,LTIMF) TRANP 48
DIMENSION WFZ(KBHF,NDATF,LTIMF) TRANP 49
DATA PROGRAM/*TRANP*/ TRANP 50
2 FORMAT(* TIME=#E12.4,*. ALT=#E12.4,*. X-POS=#E12.4,*. Y-POS=#E12.4 TRANP 51
2,*,. CELL=#I6,*. REACHED#) TRANP 52
3 FORMAT(* TIME=#E12.4,*. ALT=#E12.4,*. X-POS=#E12.4,*. Y-POS=#E12.4 TRANP 53
3,*,. CELL=#I6,*. ATTEMPTED#) TRANP 54
4 FORMAT(*OWAFER WITH INITIAL CONFIGURATION XP,YP,ZP,TP #4E12.4/*REQTRANP 55
1QUIRED CHANNELLING AT CONFIGURATION XC,YC,ZC,TC #4E12.4) TRANP 56
EPSILO=.0005 TRANP 57
EPS=EPSILO*WINT TRANP 58

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EPST=EPSILO*TOEP	TRANP 59
EPS7=.1	TRANP 60
X0=XP	TRANP 61
Y0=YP	TRANP 62
Z0=ZP	TRANP 63
T0=TP	TRANP 64
SIGX0=0.	TRANP 65
SIGY0=0.	TRANP 66
RO=0.	TRANP 67
NDATC=NDATP	TRANP 68
NDTC1=0	TRANP 69
NDT01=0	TRANP 70
KRHC1=0	TRANP 71
KRHO1=0	TRANP 72
1000 CONTINUE	TRANP 73
KAY=-1	TRANP 74
IF (KRIP.EQ.1) GO TO 50	TRANP 75
CALCULATE FALL VELOCITY FOR ADVECTION ON BASIS OF LOCAL	TRANP 76
C FALL RATE AND WIND FIELD AND STORE IN WBAR	TRANP 77
CALL CALIB(ZBH,KBHX,ZO,KAY,KBHZ)	TRANP 78
CALL CALIB(TIMUP,LTIMX,TO,1,LTIM)	TRANP 79
WBAR=WFX(KBHZ-1,NDATC,LTIM)-CAVS(KBHZ-1)	TRANP 80
IF (WBAR) 112,111,110	TRANP 81
COMPUTE THE VERTICAL PSEUDO-VELOCITY WBAR AND STORE ITS SIGN IN KAY	TRANP 82
C FOR THE DIFFUSIVE SETTLING CASE	TRANP 83
50 WBAR=(ZDEP-ZP)/(TDEF-TP)	TRANP 84
IF (WBAR) 112,111,110	TRANP 85
110 KAY=KAY+1	TRANP 86
111 KAY=KAY+1	TRANP 87
112 CONTINUE	TRANP 88
CALIBRATION OF ZDEP AGAINST ZBH YIELDS TERMINAL ZBH-PLANE	TRANP 89
IF (KRIP.EQ.1) CALL CALIB(ZBH,KBHX,ZDEP,KAY,KBH)	TRANP 90
CONSIDER KAY=0 CASE INDEPENDENTLY	TRANP 91
200 IF(KAY.NE.0) GO TO 205	TRANP 92
IF (KRIP.EQ.1) GO TO 205	TRANP 93
C IN THE ADVECTIVE TRANSPORT CASE WHENEVER THE ACTUAL FALL RATE	TRANP 94
C IS ZERO THEN SET THE DEPOSITION TIME INCREMENT EQUAL TO THE	TRANP 95
C TIME LEFT BEFORE THE WIND FIELD IS UPDATED	TRANP 96
TSEG=TIMUP(LTIM+1)-TO	TRANP 97
KBHC=KBHZ+1	TRANP 98
KRHO=KBHZ	TRANP 99
GO TO 300	TRANP100
205 TSEG=TDEF-TO	TRANP101
MODE=1	TRANP102
KRHC=KBH	TRANP103
KRHO=KBHC-1	TRANP104
GO TO 300	TRANP105
CALIBRATION OF ZO AGAINST ZBH YIELDS CURRENT ZBH-PLANE	TRANP106
206 CALL CALIB(ZBH,KBHX,ZO,-KAY,KTRY)	TRANP107
CALL CALIB(ZBH,KBHX,ZO,+KAY,KBHC)	TRANP108
IF ((KRIP.EQ.0).OR.(KRHO.NE.KTRY)) GO TO 213	TRANP109
CONSIDER EXCURSION TO TERMINAL ZBH-PLANE	TRANP110
KBHC=KRH	TRANP111
ZEST=ZBH(KBHC)	TRANP112
MODE=0	TRANP113
IF(KAY*(KRHO-KBHC)+1) 221,213,218	TRANP114
CONSIDER EXCURSION BETWEEN ADJACENT ZBH-PLANES	TRANP115
213 KRHC=KRHC+KAY	TRANP116

ZEST=ZAH(KBHC)	TRANP117
MODE=1	TRANP118
IF((KBHC.LE.KBHX).AND.(KAY*ZEST.LE.KAY*ZDEP)) GO TO 221	TRANP119
CONSIDER EXCURSION TO TERMINAL ZDEP-PLANE	TRANP120
214 KBHC=KBHO+KAY	TRANP121
ZEST=ZDEP	TRANP122
MODE=1	TRANP123
221 TSEG=(ZEST-ZO)/WBAR	TRANP124
CHECK IF UPDATE TIME BOUNDARY WILL BE CROSSED	TRANP125
300 TC=TO+TSEG	TRANP126
CALL CALIB(TIMUP,LTIMX,TO,1,LTIM)	TRANP127
IF((LTIM.LT.LTIMX).AND.(TIMUP(LTIM+1).LE.TC)) TSEG=TIMUP(LTIM+1)-TO	TRANP128
COMPUTE AVERAGE HORIZONTAL VELOCITIES UBAR AND VBAR	TRANP129
KDHA=KBHO	TRANP130
KBHB=KBHC	TRANP131
IF(KAY.LT.0) GO TO 405	TRANP132
KBHA=KBHC	TRANP133
KBHB=KBHO	TRANP134
405 CALL GETDA(USUM,ZRH,KBHA,KBHB,NDATC,LTIM,UBAR,KRHF,NDATF,LTIMF)	TRANP135
CALL GETDA(VSUM,ZRH,KBHA,KBHB,NDATC,LTIM,VBAR,KRHF,NDATF,LTIMF)	TRANP136
407 IF(NDEP.EQ.0) GO TO 412	TRANP137
COMPUTE AVERAGE HORIZONTAL DISPERSION AND WIND ORIENTATION ANGLE	TRANP138
CALL GETDA(DXSUM,ZRH,KBHA,KBHB,NDATC,LTIM,DXBAR,KRHF,NDATF,LTIMF)	TRANP139
CALL GETDA(DYSUM,ZRH,KBHA,KBHB,NDATC,LTIM,DYBAR,KRHF,NDATF,LTIMF)	TRANP140
CALL GETDA(RSUM,ZRH,KBHA,KBHB,NDATC,LTIM,RBAR,KRHF,NDATF,LTIMF)	TRANP141
RC=RO+RBAR	TRANP142
SIGXC=SIGXO+DXBAR*TSEG	TRANP143
SIGYC=SIGYO+DYBAR*TSEG	TRANP144
COMPUTE CURRENT POSITION AND TIME (XC,YC,ZC,TC)	TRANP145
412 TC=TO+TSEG	TRANP146
ZC=ZO+WBAR*TSEG	TRANP147
XC=XO+UBAR*TSEG	TRANP148
YC=YO+VBAR*TSEG	TRANP149
CALL NEST(NET,METSU,XC,YC,NDATC,XL,XR,YL,YU,ICF,JCF,NCF)	TRANP150
IF(MC(4).EQ.1) WRITE(ISOUP,3) TC,ZC,YC,NDATC	TRANP151
COMPARE CURRENT MESH INDEX NDATC WITH PREVIOUS MESH INDEX NDAT0	TRANP152
IF(NDATC.EQ.NDAT0) GO TO 700	TRANP153
COMPUTE INTERPOLATED POINT	TRANP154
XT=XC	TRANP155
YT=YC	TRANP156
ZT=ZC	TRANP157
IF(NODE.EQ.0) GO TO 213	TRANP158
CALL BCUN(NET,METSU,XT,YT,XO,YO,XC,YC,ICF,JCF,NCF)	TRANP159
ZC=SOPT((XT-XO)**2+(YT-YO)**2)/((XT-XO)**2+(YT-YO)**2)	TRANP160
ZC=ZT+ZC*(ZO-ZT)	TRANP161
IF(ABS(WBAR).LE.1.0E-30) GO TO 510	TRANP162
TSEG=(ZC-ZO)/WBAR	TRANP163
GO TO 518	TRANP164
510 IF(ABS(UBAR).LE.1.0E-30) GO TO 513	TRANP165
TSEG=(XC-XO)/UBAR	TRANP166
GO TO 518	TRANP167
513 IF(ABS(VBAR).LE.1.0E-30) GO TO 516	TRANP168
TSEG=(YC-YO)/VBAR	TRANP169
GO TO 518	TRANP170
516 CALL ERROR(PROGPM,516,ISOUP)	TRANP171
RETURN	TRANP172
518 IF(NDEP.NE.0) GO TO 521	TRANP173
RC=RO+RBAR	TRANP174

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SIGXC=SIGXO+DXBAR*TSEG
SIGYC=SIGYO+DYBAR*TSEG
521 TC=TO+TSEG
CALL NEST(NET,NETSU,XC,YC,NDATC,XL,XR,YL,YU,ICF,JCF,NCF)
CHECK IF PARCEL CENTER POSITION IS OSCILLATING
IF((K9H01.NE.K9H01).OR.(K9HC1.NE.K9HC1).OR.(NDTC1.NE.NDATC1).OR.
1(NDT01.NE.NDAT01)) GO TO 626
IF(MC(4).EQ.1) WRITE(ISOOT,4) XP,YP,ZP,TP,XC,YC,ZC,TC
CALL CNTR(NET,NETSU,NDAT0,XG,YG,ICF,JCF,NCF)
XQ=XG
YQ=YG
CALL NEST(NET,NETSU,XQ,YQ,NDATQ,XLO,XRO,YLO,YUO,ICF,JCF,NCF)
CLEAR STORED MESH AND STRATUM INDICES
NDTC1=0
NDT01=0
K9HC1=0
K9H01=0
CHANNEL WAFER CENTER POSITION ALONG APPROPRIATE CELL BOUNDARY
SPE=2.*EPS
IF((ABS(XLO-XR).GT.SPE).AND.(ABS(XRO-XL).GT.SPE)) GO TO 616
UBAR=0
CALL GETDA(VSUM,ZRF,K9PA,K9PB,NDAT0,LTIM,UBARC,K9HF,NDATF,LTIMF)
IF(ABS(UBARC).LE.ABS(UBAR)) GO TO 407
UBAR=UBARC
NDAT0=NDATC
GO TO 407
616 IF((ABS(YLO-YU).GT.SPE).AND.(ABS(YUO-YL).GT.SPE))
1CALL ERROR(PROGPM,616,ISOOT)
UBAR=0
CALL GETDA(USUM,ZRF,K9PA,K9PB,NDAT0,LTIM,UBARC,K9HF,NDATF,LTIMF)
IF(ABS(UBARC).LE.ABS(UBAR)) GO TO 407
UBAR=UBARC
NDATC=NDATC
GO TO 407
COMMIT PREVIOUS AND CURRENT MESH AND STRATUM INDICES TO STORAGE
626 NDTC1=NDAT0
NDT01=NDATC
K9HC1=K9HC
K9H01=K9H0
CONVERT XO,YC,ZC,TO,SIGXO,SIGYO, AND NDATC TO CURRENT VALUES
700 ZO=ZC
XO=XC
YO=YC
TO=TC
NDAT0=NDATC
IF(MC(4).EQ.1) WRITE(ISOOT,2) TO,ZC,XO,YO,NDAT0
IF(NDER.NE.0) GO TO 709
SIGXC=SIGXC
SIGYC=SIGYC
RO=RC
CHECK IF CURRENT POSITION IS OUTSIDE ATMOSPHERE
708 IF(NDAT0.LE.0) GO TO 710
IF(KRIP.EQ.1) GO TO 709
C IF DEPOSITION PLANE IS REACHED OR TRANSPORT TIME LIMIT IS EXCEEDED
C EXIT FROM TRANP, OTHERWISE RETURN TO TOP
IF((70-ZDEP).LE.EPS2).OR.(5*INSX-(G).LE.EPS1) GO TO 724
GO TO 1046
709 CONTINUE

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TRANP175
TRANP176
TRANP177
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CHECK IF TOTAL FLIGHT TIME HAS BEEN EXHAUSTED
IF (TO+EPST-TDEP) 200,720,720
CARRY PARCEL CENTER BACK INTO AT40S. IF NDEP IS NOT EQUAL TO ZERO
710 IF (NDEP.EQ.0) GO TO 720
    XO=XO-2.*EPS.
    YO=YO-2.*EPS
    CALL NEST(NET,NETSU,XO,YO,NDATO,XL,YR,YL,YU,ICF,JCF,NCF)
    IF (NDATO.GT.0) GO TO 720
714 XO=XO+4.*EPS
    YO=YO+4.*EPS
    CALL NEST(NET,NETSU,XO,YO,NDATO,XL,YR,YL,YU,ICF,JCF,NCF)
    IF (NDATO.LE.0) CALL ERROR(PROGFM,720,ISOUT)
COMPUTE HORIZ. DISPERSION IF NDEP IS NOT EQUAL TO ZERO
720 IF (NDEP.NE.0) RETURN
    P2=PWAF**2
    IF (MC(10).EQ.1) GO TO 721
    SIGXC=2.*DOWN*SIGXC
    SIGYC=2.*CROSS*SIGYC
    GO TO 722
721 TRIP=TC-TP
    DSPRTX=SIGXO/TRIP
    TONEX=4.*((R2/DSPRTX)**(1./3.))
    IF (TRIP.LE.TONEX) SIGXU=DSPRTX*TONEX*(TRIP**2)/3.
    IF (TRIP.GT.TONEX) SIGXC=DSPRTX*(TRIP**3)/3.
    SIGXO=SIGXO*(DOWN** (3./2.))
    DSPRTY=SIGYO/TRIP
    TONEY=4.*((R2/DSPRTY)**(1./3.))
    IF (TRIP.LE.TONEY) SIGYC=DSPRTY*TONEY*(TRIP**2)/3.
    IF (TRIP.GT.TONEY) SIGYC=DSPRTY*(TRIP**3)/3.
    SIGYO=SIGYO*(CROSS** (3./2.))
722 SIGXO=SQRT(R2+SIGXO)
    SIGYO=SQRT(R2+SIGYO)
    RETURN
END

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